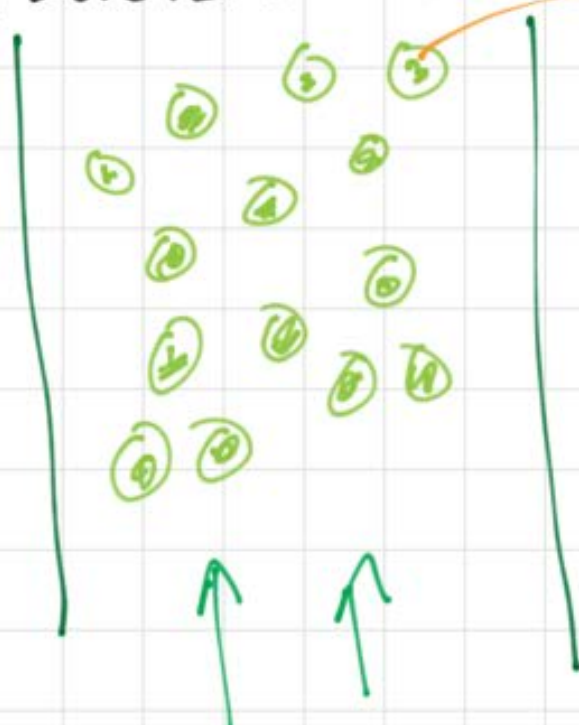


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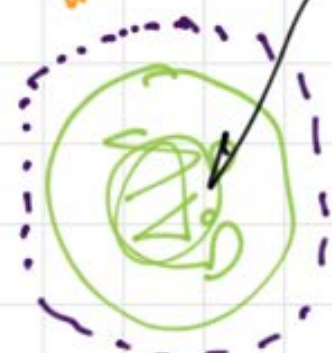
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CONTINUED DISCUSSION OF BOUNDARY-LAYERS FLUIDIZED BED REACTOR

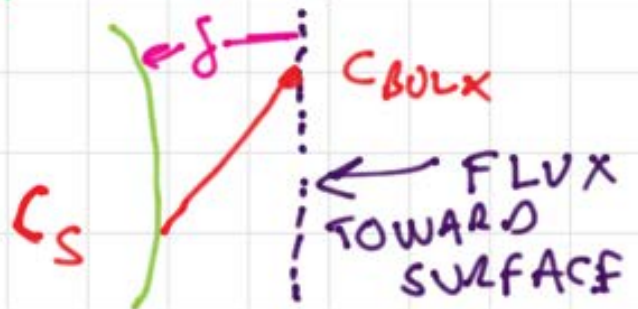


REACTANT FLOW
 H_2, C_mH_{2m-x}

SOLID CATALYST



NEED TO KNOW HOW FAST H_2 & C_mH_n GET FROM BULK GAS TO SURFACE OF CATALYST



$$\text{FLUX} \equiv D \frac{(C_B - C_S)}{\delta} = h(C_B - C_S)$$

MOLECULAR DIFFUSIVITY

KEY QUESTION: VALUE OF δ

6. Past single spheres	Sc = 0.6 - 3200	Sh = Sh ₀ + 0.347(Re ⁿ Sc ^{0.5}) ^{0.62}	
	Re ⁿ Sc ^{0.5} = 1.8 - 600 000	Sh ₀ = $\begin{cases} 2.0 + 0.569(Gr_D Sc)^{0.250} & Gr_D Sc < 10^8 \\ 2.0 + 0.0254(Gr_D Sc)^{0.333} Sc^{0.244} & Gr_D Sc > 10^8 \end{cases}$	55

$$Sh \equiv \frac{hd}{D} \leftarrow \text{PARTICLE DIAMETER}$$

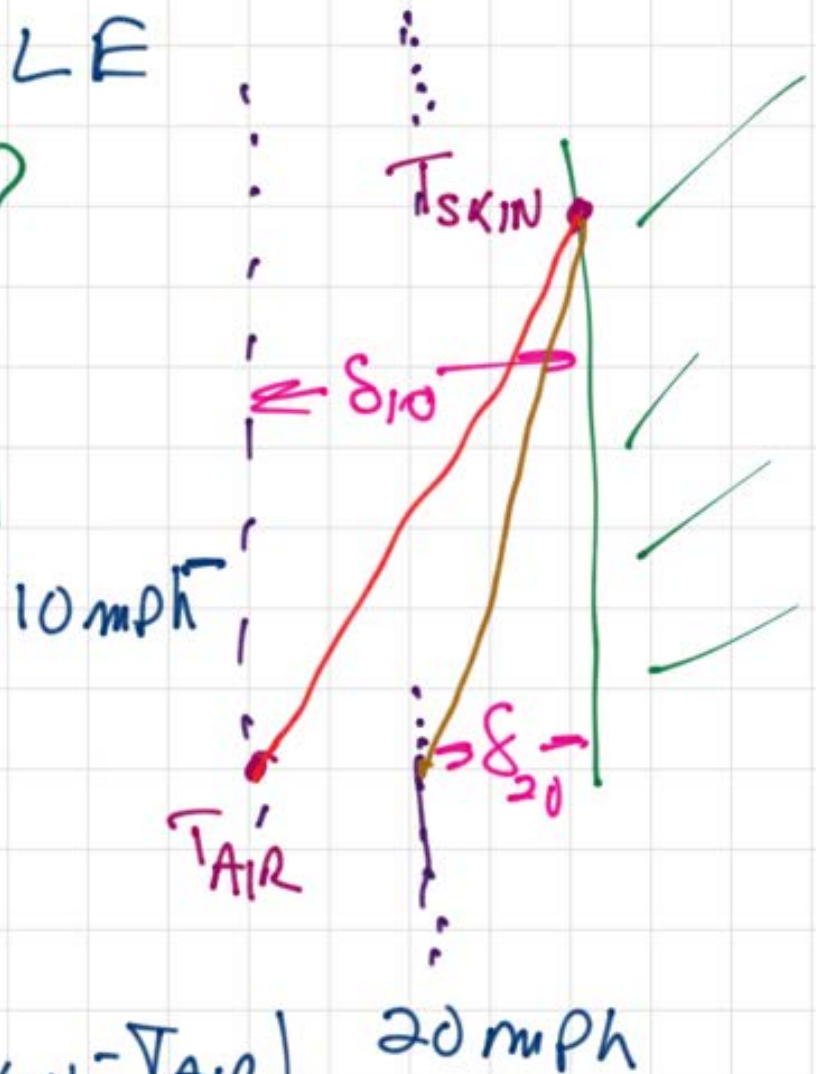
$$Sh = 2 + .347 Re^{.62} Sc^{.3}$$

FIND Re, Sc = $\frac{\nu}{D}$

CALCULATE SH,
GET h

$$\delta = \frac{D}{h}$$

WIND CHILL IS ANOTHER EXAMPLE



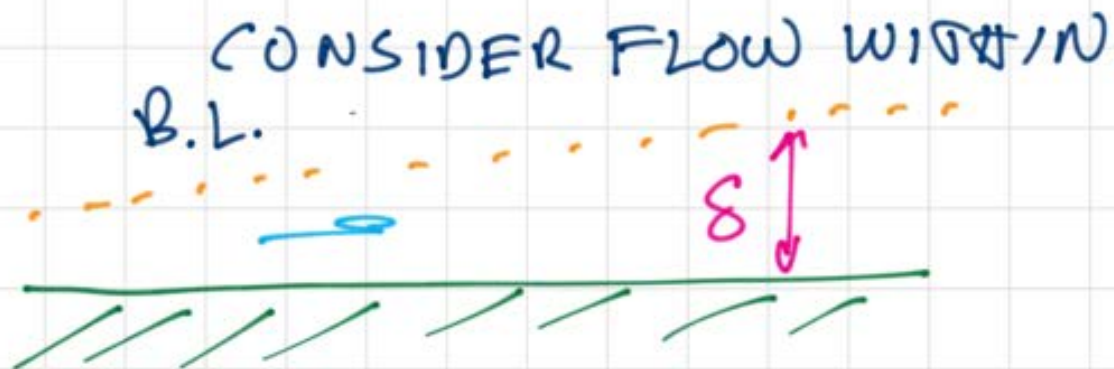
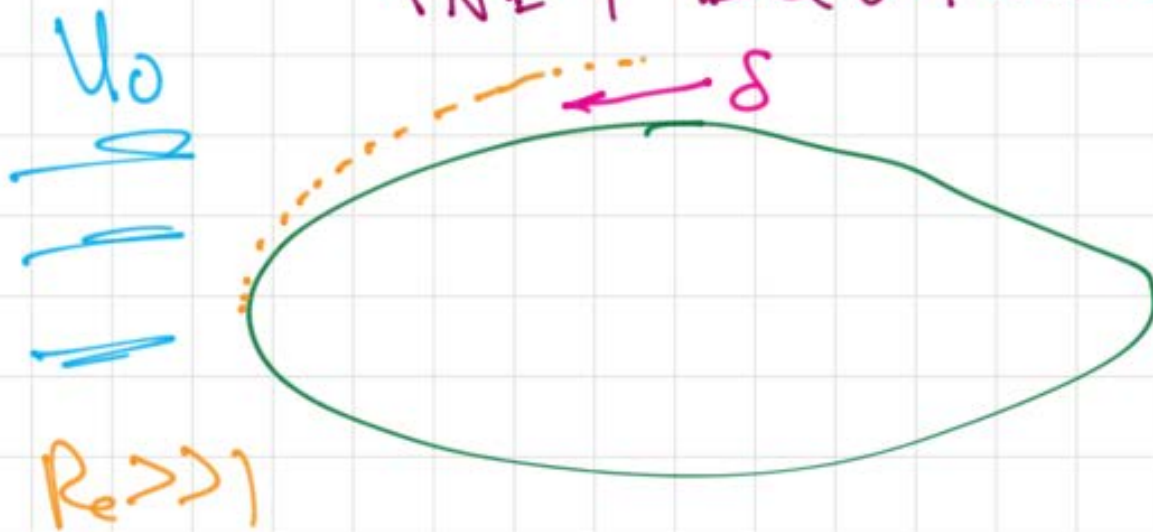
$$FLUX \hat{=} Q \frac{(T_{SKIN} - T_{AIR})}{\delta}$$

THERMAL DIFFUSIVITY $Nu = \frac{hd}{\alpha}, h = \frac{\alpha}{\delta}$

5. Perpendicular to single cylinders	$Re = 400 - 25\,000$	$\frac{k_G Pr}{G_M} Sc^{0.56} = 0.281 Re^{0.4}$	5
	$Sc = 0.6 - 2.6$		
	$Re' = 0.1 - 10^5$		16,
	$Pr = 0.7 - 1500$	$Nu = (0.35 + 0.34 Re^{0.5} + 0.15 Re^{0.58}) Pr^{0.3}$	21,
			42

ANALYSIS OF NAVIER-STOKES EQUATIONS FOR A BOUNDARY-LAYER FLOW:

CAN WE LEARN ANYTHING WITHOUT ACTUALLY SOLVING THE EQUATIONS?



PHYSICAL PRINCIPLE:

INERTIA & VISCOUS TERMS ARE BOTH IMPORTANT

NONDIMENSIONALIZE NAVIER STOKES EQUATIONS

$$v_x^* \equiv \frac{v_x}{U_0}, \quad v_y^* \equiv \frac{v_y}{U_0} \dots$$

$$x^* \equiv \frac{x}{L}, \quad y^* \equiv \frac{y}{L}$$

$$p^* \equiv \frac{p}{\rho U_0^2} \dots$$

$$\frac{\partial \vec{v}^*}{\partial t^*} + \vec{v}^* \cdot \nabla^* \vec{v}^* = -\nabla^* p^* + \frac{1}{Re} \nabla^{*2} \vec{v}^*$$

$$\text{As } Re \rightarrow \infty$$

$$\frac{\partial \vec{v}^*}{\partial t^*} + \vec{v}^* \cdot \nabla^* \vec{v}^* = -\nabla^* p^*$$

WE HAVE TO MAKE AN ALTERATION IN OUR ANALYSIS TO KEEP VISCOUS TERMS !!

CHANGE EQUATION TO:

$$x^* = \frac{x}{L}$$

$$y^* = \frac{y}{\delta}$$

ADDITIONAL LENGTH SCALE

$$v_x^* = \frac{v_x}{U_0}$$

$$v_y^* = \frac{v_y}{V}$$

ADDITIONAL VELOCITY SCALE ..

SUBSTITUTE INTO
CONTINUITY

$$\frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} = 0$$

$$\frac{U_0}{L} \frac{\partial v_x^*}{\partial x^*} + \frac{V}{\delta} \frac{\partial v_y^*}{\partial y^*} = 0$$

$\underbrace{\hspace{10em}}_{\mathcal{O}(1)} \quad \underbrace{\hspace{10em}}_{\mathcal{O}(1)}$

TO MAKE
THIS
WORK

THUS: $V \sim \frac{\delta}{L} U_0$

WE EXPECT A "WEAK" FLOW
NORMAL TO SURFACE, $v_y \sim v_x \frac{\delta}{L}$

NOW:

RE-NONDIMENSIONALIZE
NAVIER-STOKES EQUATIONS
WITH $U_0, L, V, \delta \dots$

X-N.S EQUATION:

$$\rho \left(u_0 v_x^* \frac{u_0}{L} \frac{\partial v_x^*}{\partial x^*} + v v_y^* \frac{u_0}{\delta} \frac{\partial v_x^*}{\partial y^*} \right) =$$

$$-\frac{\rho u_0^2}{L} \frac{\partial p^*}{\partial x^*} + \mu \left(\frac{u_0}{L^2} \frac{\partial^2 v_x^*}{\partial x^{*2}} + \frac{u_0}{\delta^2} \frac{\partial^2 v_x^*}{\partial y^{*2}} \right)$$

CLEAR VARIABLES TO LEFT

$$\frac{\rho \delta^2 u_0}{\mu L} \left(v_x^* \frac{\partial v_x^*}{\partial x} + v_y^* \frac{\partial v_x^*}{\partial y} \right) = -\frac{\partial p^*}{\partial x^*} + \frac{\partial^2 v_x^*}{\partial y^{*2}}$$

FOR OUR ANALYSIS TO WORK WE REQUIRE:

$$\frac{\rho \delta^2 u_0}{\mu L} = O(1)$$

THUS: $\delta^2 = \frac{\mu L}{\rho u_0}$

KEY

RESULT!!

$$\boxed{\frac{\delta}{L} = \frac{1}{\sqrt{Re}}}$$

$$Re = \frac{L u_0 \rho}{\mu}$$

BOUNDARY-LAYER THICKNESS

y-DIRECTION.

USE SAME ANALYSIS!

$$\frac{\partial P}{\partial y} = O(\delta) \approx 0$$

BOUNDARY-LAYER EQUATIONS

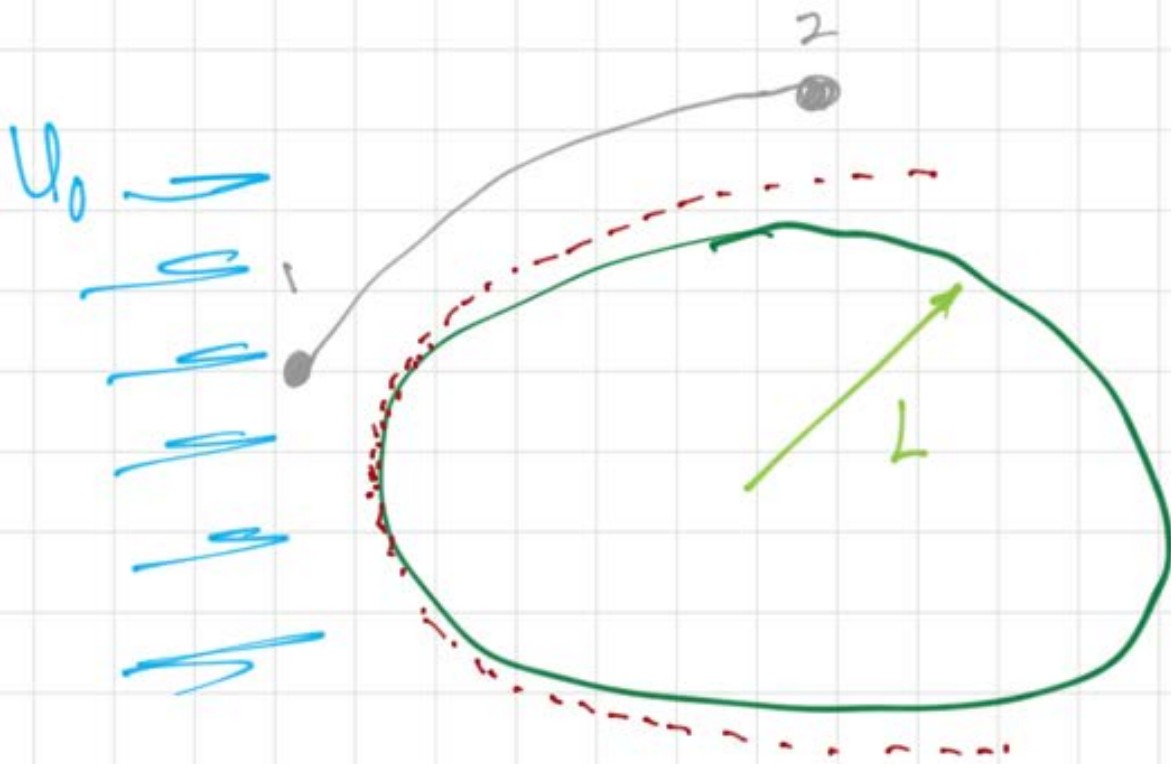
$$\frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} = 0$$

$$v_x \frac{\partial v_x}{\partial x} + v_y \frac{\partial v_x}{\partial y} = -\frac{1}{\rho} \frac{\partial P}{\partial x} + \frac{\mu}{\rho} \frac{\partial^2 v_x}{\partial y^2}$$

$$\frac{\partial P}{\partial y} = 0$$

→ SO THAT WE CAN GET PRESSURE
INSIDE BOUNDARY-LAYER FROM
BERNOULLI EQUATION JUST ABOVE
SURFACE

$$\Delta \left(\frac{U^2}{2} + gh + \frac{P}{\rho} \right) = 0$$



FOR $1 \rightarrow 2$ $\Delta \left(\frac{V^2}{2} + gh + \frac{P}{\rho} \right) = 0$

BERNOULLI

INSIDE BOUNDARY-LAYER

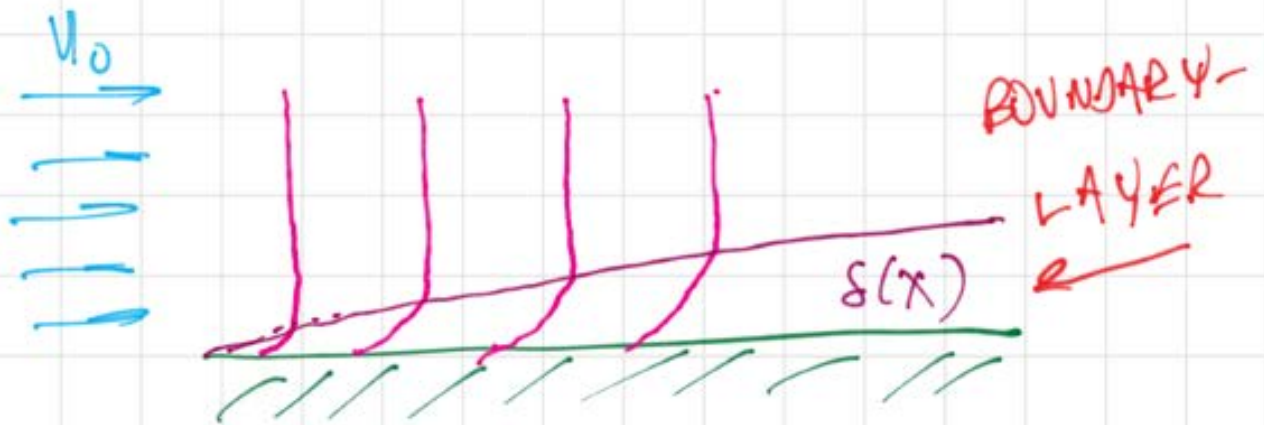
BOUNDARY-LAYER

$$\frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} = 0$$

EQUATIONS $v_x \frac{\partial v_x}{\partial x} + v_y \frac{\partial v_x}{\partial y} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + \frac{\mu}{\rho} \frac{\partial^2 v_x}{\partial y^2}$

$$\frac{\partial p}{\partial y} = 0$$

WE WANT TO ANALYZE:



BOUNDARY-LAYER

$$\frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} = 0$$

EQUATIONS $v_x \frac{\partial v_x}{\partial x} + v_y \frac{\partial v_x}{\partial y} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + \frac{\mu}{\rho} \frac{\partial^2 v_x}{\partial y^2}$

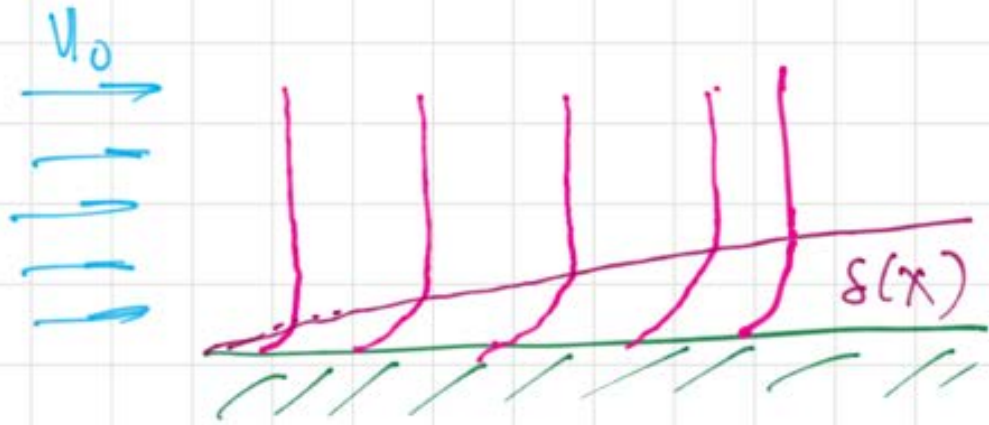
$$\frac{\partial p}{\partial y} = 0$$

CONSIDER "FLAT PLATE"

$$\Delta \left(\frac{U^2}{2} + gh + \frac{P}{\rho} \right) = 0$$

$$U_1 = U_2 \quad P_1 = P_2 \quad \therefore \frac{\partial P}{\partial x} = 0$$

STILL HAVE COUPLED, NONLINEAR PDE'S ... - CAN WE SIMPLIFY?



SUPPOSE THAT THIS CARTOON HAS
SOME REAL INSIGHT

- NO GEOMETRIC LENGTH
SCALE FOR BOUNDARY
- LAYER
- COULD THE PROFILES
BE SELF SIMILAR?

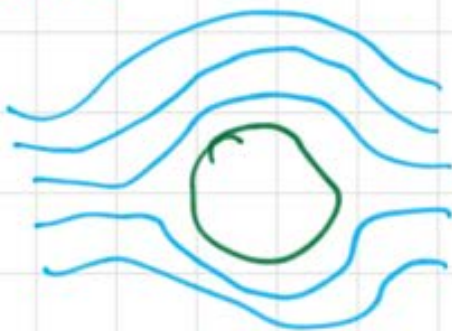
IF THE PROFILES ARE SELF-SIMILAR THEN AS WE PROGRESS IN DISTANCE THERE IS A RELATIONSHIP BETWEEN x + y AS:

$\eta \Rightarrow$ SIMILARITY VARIABLE

ONLY LENGTH SCALE TO MAKE $\rightarrow \eta \equiv \frac{y}{\sqrt{\nu x / u_0}}$ \leftarrow APPARENT CHANGE IN ϵ w/ DISTANCE

WE WILL ALSO USE THE "STREAM FUNCTION", ψ

DEFINED FROM CONTINUITY $\int \left(v_x \equiv \frac{\partial \psi}{\partial y}, \quad v_y \equiv -\frac{\partial \psi}{\partial x} \right)$



LINES OF $\psi = \text{CONSTANT}$

$\psi(x, y) \equiv f(\eta) \sqrt{\nu x u_0}$

FROM THIS:

$$v_x = \frac{\partial \psi}{\partial y} = \frac{\partial \psi}{\partial \eta} \frac{\partial \eta}{\partial y}$$

$$v_y = -\frac{\partial \psi}{\partial x} = -\frac{\partial \psi}{\partial \eta} \frac{\partial \eta}{\partial x} \dots$$

$$f'''(\eta) + \frac{1}{2} f(\eta) f''(\eta) = 0$$

BC's

$$f(\eta) = 0 \quad v_y(y=0, x) = 0$$

$$f'(\eta) = 0 \quad v_x(y=0, x) = 0$$

$$f'(\infty) = 1 \quad \begin{cases} v_x(x=0, y) = U_0 \\ v_x(y, y=\infty) = U_0 \end{cases}$$

SOLVE BY SHOOTING METHOD

BOUNDARY-LAYER THICKNESS

IS ABOUT $\eta = 5$

SO, WHAT IS y VALUE OF δ ?

$$\frac{y}{\sqrt{\frac{xv}{u_0}}} = 5 \quad \therefore \quad \delta = 5 \sqrt{\frac{xv}{u_0}}$$

$$\delta = 5x \sqrt{\frac{v}{xu_0}}$$

$$\frac{\delta}{x} = \frac{5}{\sqrt{Re_x}} \quad Re_x \equiv \frac{xu_0}{v}$$

WHAT IS WALL SHEAR STRESS?

$$\tau_w = \mu \frac{\partial v_x}{\partial y} = \mu u_0 \left(\frac{u_0}{xv} \right)^{1/2} f''(0)$$

$$\tau_w = .332 \mu u_0 \left(\frac{u_0}{vx} \right)^{1/2}$$

COMPARE TO:

$$\tau_w = \mu \frac{u_0}{\delta} \dots$$

$$\tau_w = \mu \frac{u_0}{5x Re_x^{-1/2}}$$

$$= .2 \mu u_0 \left(\frac{u_0}{\nu x} \right)^{1/2}$$

SO, .2 COMPARED TO
.33 IS PRETTY
CLOSE!!

WHAT IS EFFECT OF
PRESSURE GRADIENT ON
BOUNDARY-LAYER?

BERNOULLI EQ.

$$\Delta \left(\frac{V^2}{2} + gh + \frac{P}{\rho} \right) = 0$$

$$P \equiv P + \rho gh$$

THEN DIFFERENTIATE:

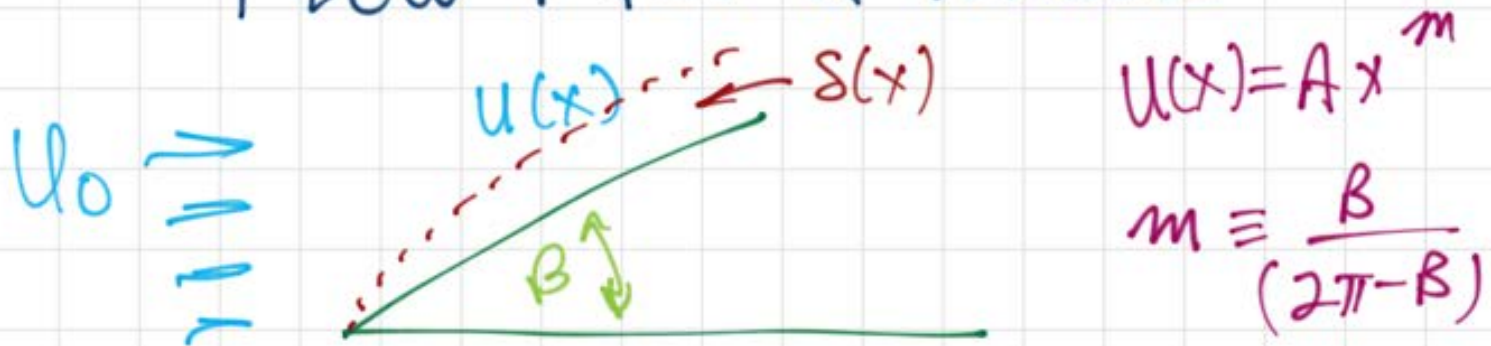
$$V \frac{dV}{dx} + \frac{1}{\rho} \frac{dP}{dx} = 0$$

CHANGE IN
FAR AWAY
FLOW

REPLACE
 $\frac{dP}{dx}$ IN
BOUNDARY-LAYER EQ

$$u_x \frac{\partial v_x}{\partial x} + v_y \frac{\partial v_x}{\partial y} = \underbrace{u \frac{du}{dx}} + v \frac{\partial^2 v_x}{\partial y^2}$$

FLOW PAST A WEDGE



INCLUDE THIS NEW TERM IN ANALYSIS:

$$f''' + \frac{m+1}{2} f f'' + m(1-f'^2) = 0$$

SYSTEM OF ODE'S:

$$y_1' = y_2$$

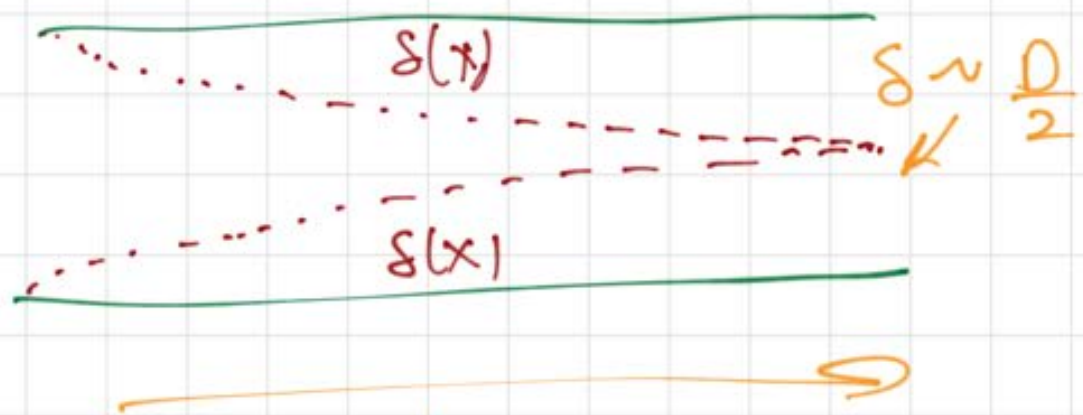
$$y_2' = y_3$$

$$y_3' = -\frac{m+1}{2} y_1 y_3 + m(1-y_2^2)$$

SOLVE

SEE "BOUNDARY LAYER . . . 2016"

LET US EXTEND THE
DEVELOPING BOUNDARY-
LAYER ON A PLATE TO
DEVELOPING LAMINAR FLOW
IN A PIPE (OR CHANNEL)



ENTRANCE LENGTH: l_e

$$\frac{D}{4} = \delta = 5x \sqrt{\frac{\nu}{x u_0}} \quad x \rightarrow l_e$$

$$\frac{D^2}{4} = 25 \frac{\nu l_e}{u_0}$$

$$\frac{l_e}{D} \sim \frac{1}{100} \frac{u_0 D}{\nu} = 0.01 Re$$