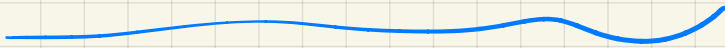


CBE 40445

9/16/20

# HETEROGENEOUS CATALYSIS

SOME REVIEW



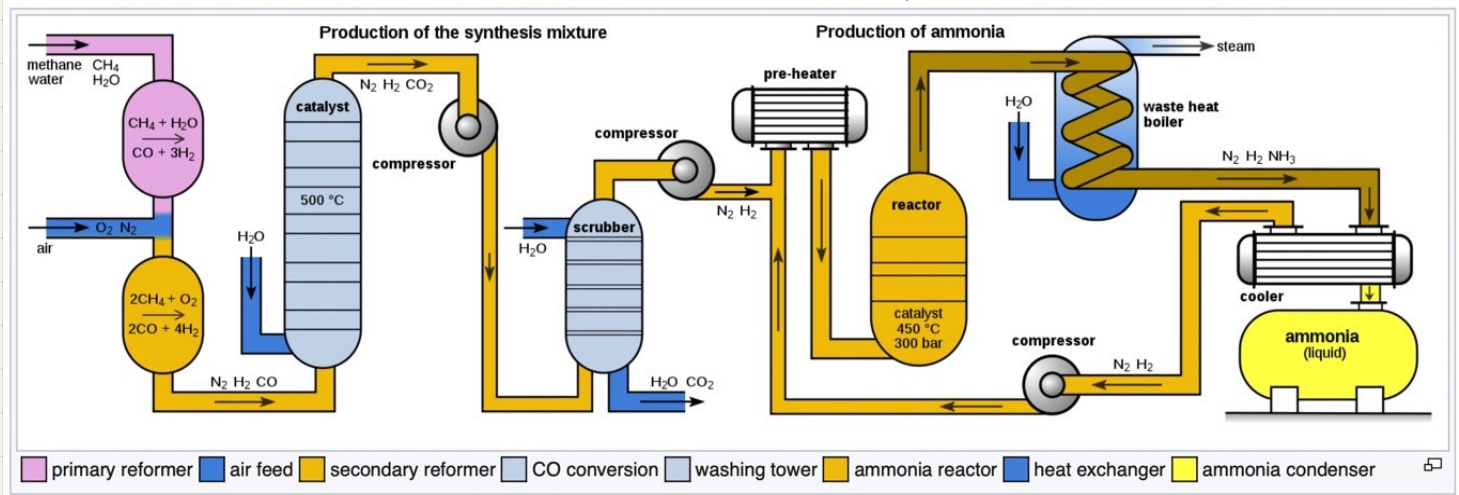
$\Delta H = -92 \text{ kJ/mole}$  AT RXN TEMP

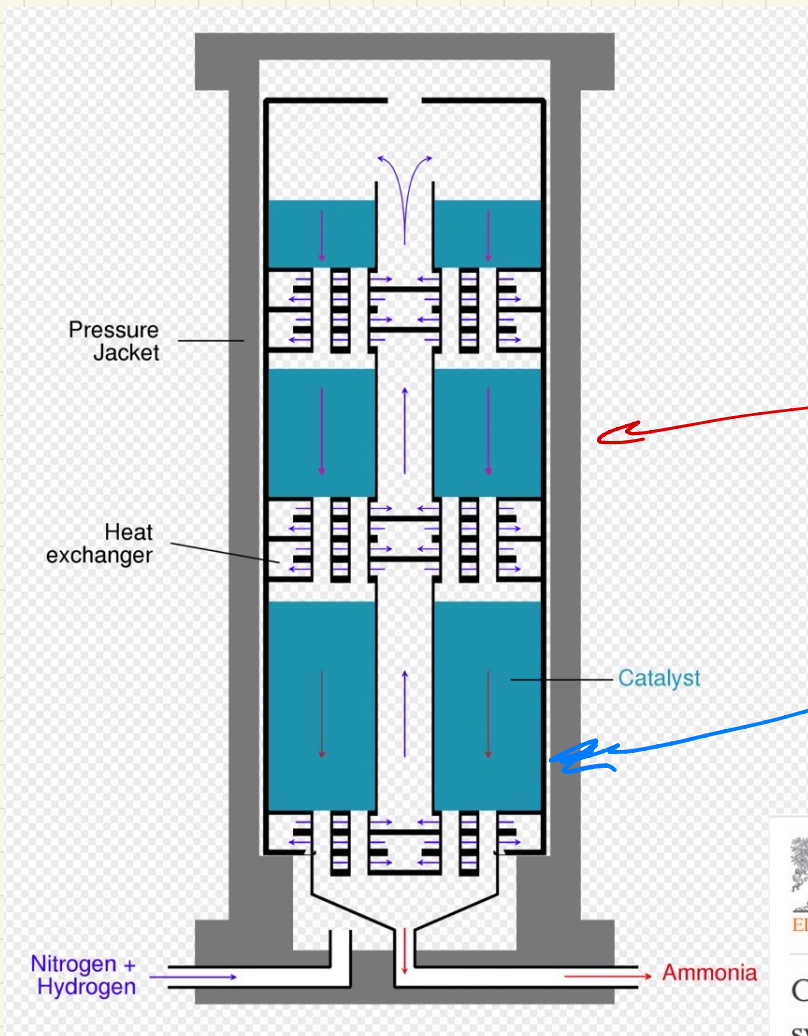
Process	Catalyst	Equation
Making ammonia	Iron	$\text{N}_2(\text{g}) + 3\text{H}_2(\text{g}) \rightleftharpoons 2\text{NH}_3(\text{g})$
Making synthesis gas (carbon monoxide and hydrogen)	Nickel	$\text{CH}_4(\text{g}) + \text{H}_2\text{O}(\text{g}) \rightleftharpoons \text{CO}(\text{g}) + 3\text{H}_2(\text{g})$
Catalytic cracking of gas oil	Zeolite	Produces: a gas (e.g. ethene, propene) a liquid (e.g. petrol) a residue (e.g. fuel oil)
Reforming of naphtha	Platinum and rhenium on alumina	$\text{CH}_3\text{CH}_2\text{CH}_2\text{CH}_2\text{CH}_2\text{CH}_3(\text{g}) \rightarrow \text{C}_6\text{H}_{12}(\text{g}) + \text{H}_2(\text{g})$
Making epoxyethane	Silver on alumina	$\text{C}_2\text{H}_4(\text{g}) + \frac{1}{2}\text{O}_2(\text{g}) \rightarrow \text{H}_2\text{C}-\text{O}-\text{CH}_2(\text{g})$
Making sulfuric acid	Vanadium(V) oxide on silica	$\text{SO}_2(\text{g}) + \frac{1}{2}\text{O}_2(\text{g}) \rightarrow \text{SO}_3(\text{g})$
Making nitric acid	Platinum and rhodium	$4\text{NH}_3(\text{g}) + 5\text{O}_2(\text{g}) \rightarrow 4\text{NO}(\text{g}) + 6\text{H}_2\text{O}(\text{g})$

Table 1 Examples of industrial processes using heterogeneous catalysis.

<https://www.essentialchemicalindustry.org/processes/catalysis-in-industry.html>

FROM WIKIPEDIA





$T \sim 350\text{ C}$

$P \sim 200\text{ ATM}$

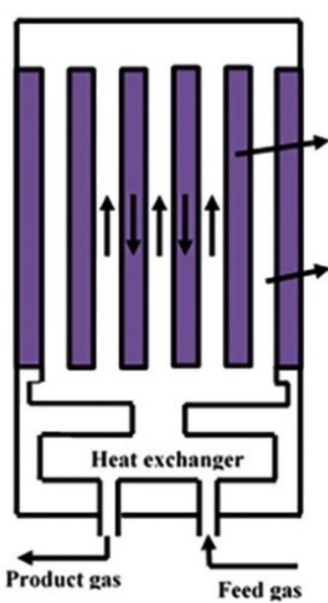
HIGHLY EXOTHERMIC

APPROACHES EQUILIBRIUM

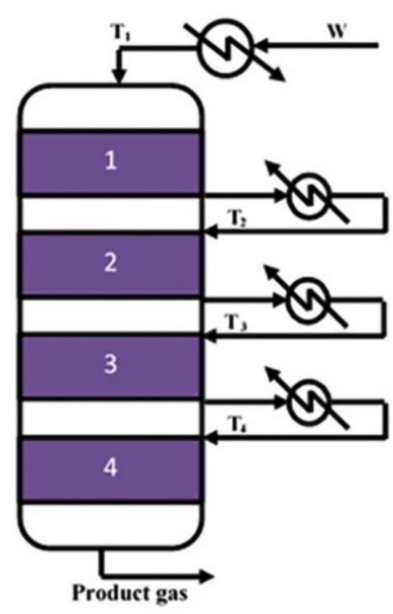
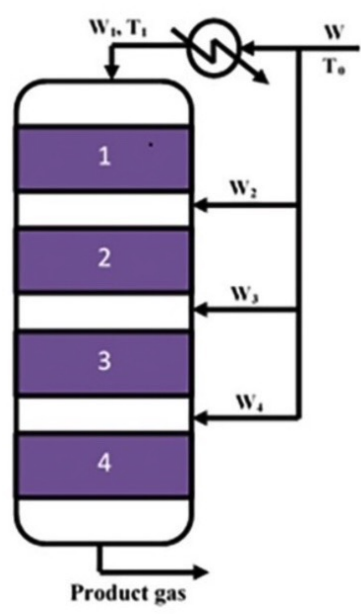


Comparison between three types of ammonia synthesis reactor configurations in terms of cooling methods

Mohammad Hasan Khademi, Reyhaneh Sadat Sabbaghi



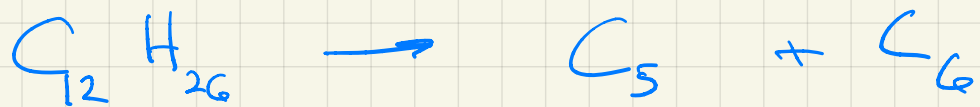
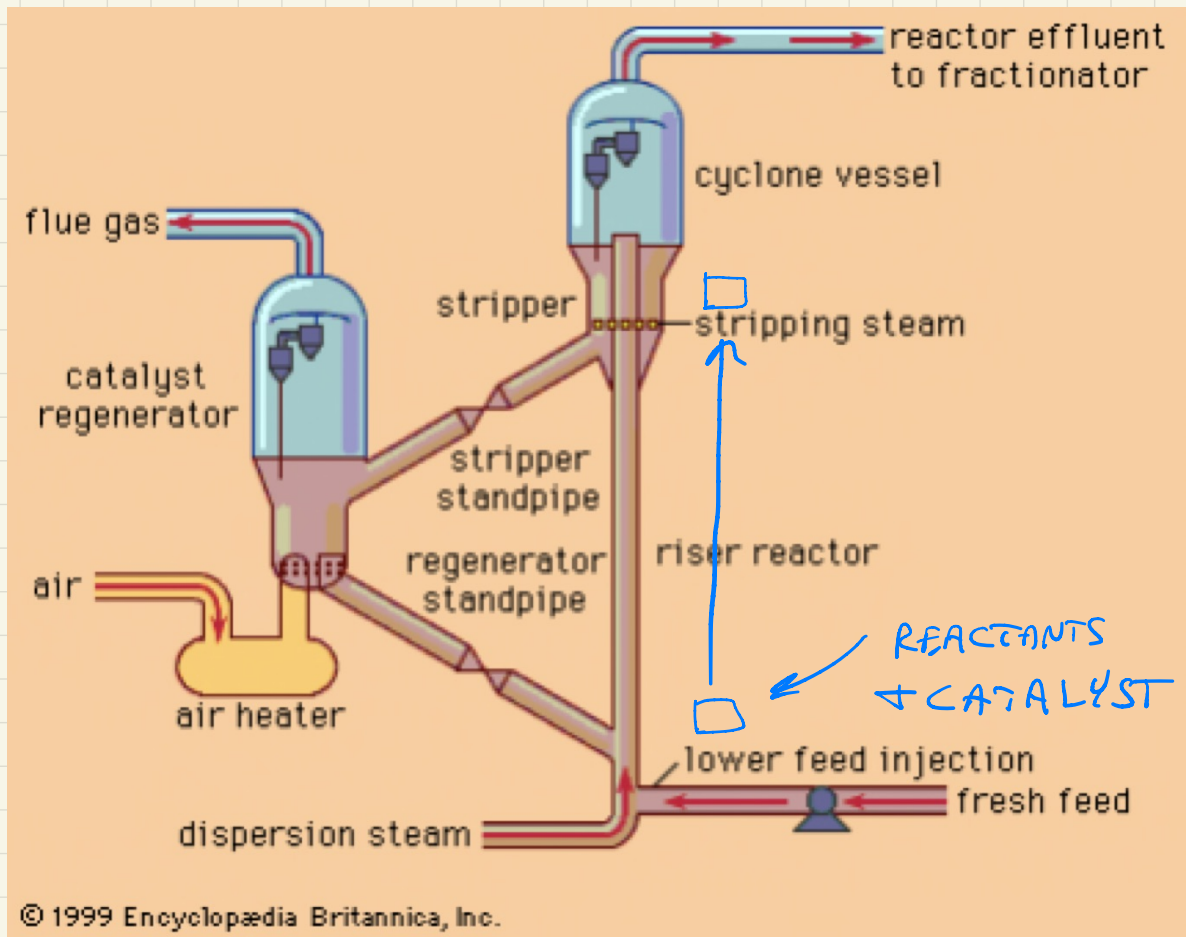
Catalyst zone  
Cooling Tube



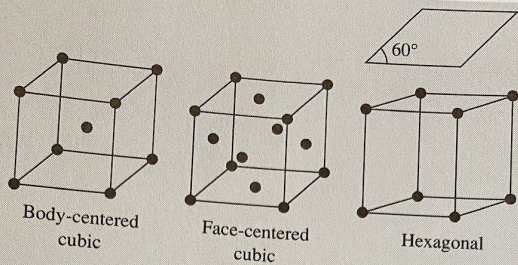
Internal direct cooling reactor, IDCR) (Adiabatic quench cooling reactor, AQCR) (Adiabatic indirect cooling reactor, AICR)



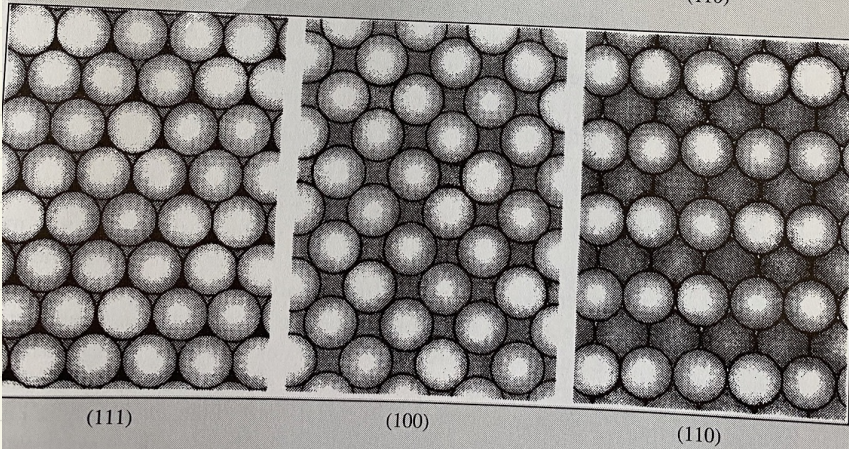
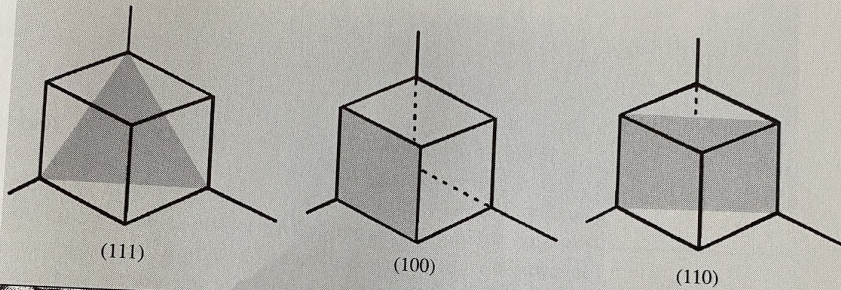
# CATALYTIC CRACKING



ENDOTHERMIC



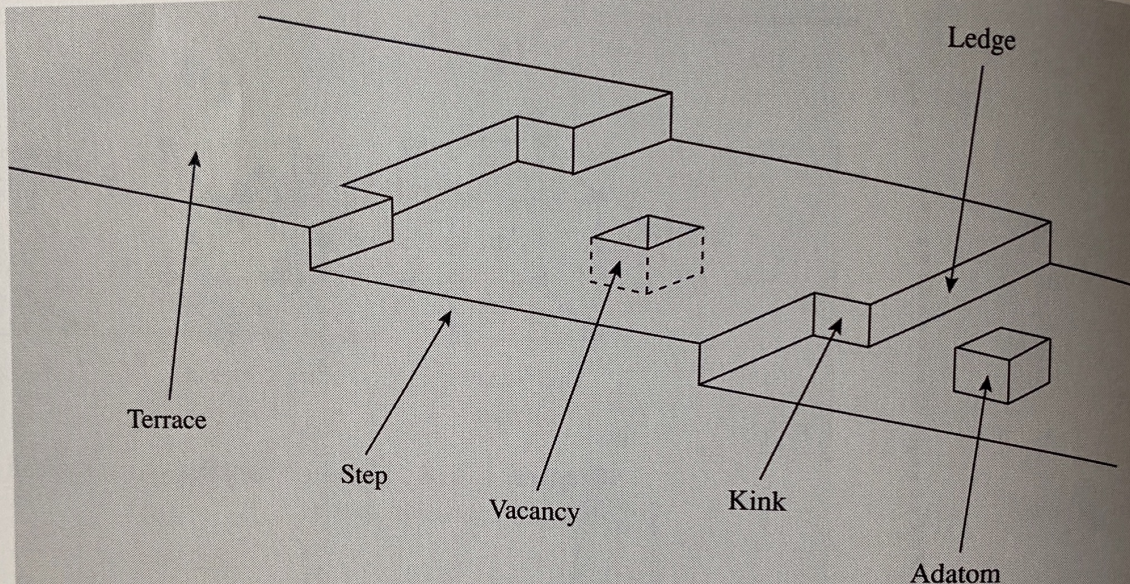
**Figure 5.1.2** | Crystal structures of catalytically relevant transition metals.



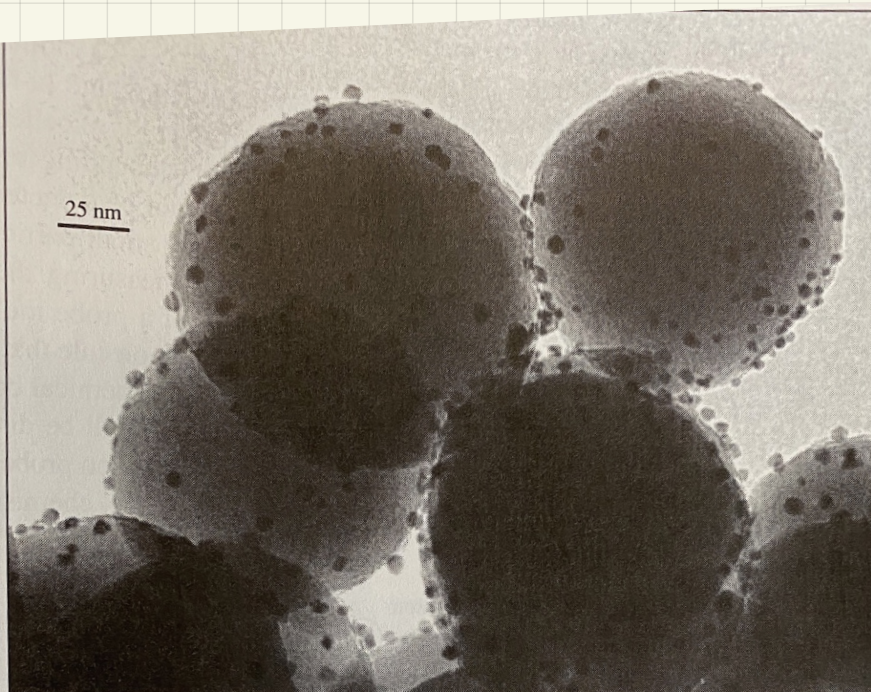
**Figure 5.1.3** | Atomic arrangements of the low-index surface planes of an FCC crystal. Adapted from R. Masel, *Principles of Adsorption and Reaction on Solid Surfaces*, Wiley, New York, copyright © 1996, p. 38, by permission of John Wiley & Sons, Inc.)

Single crystal surfaces are associated with planes in the unit cell.

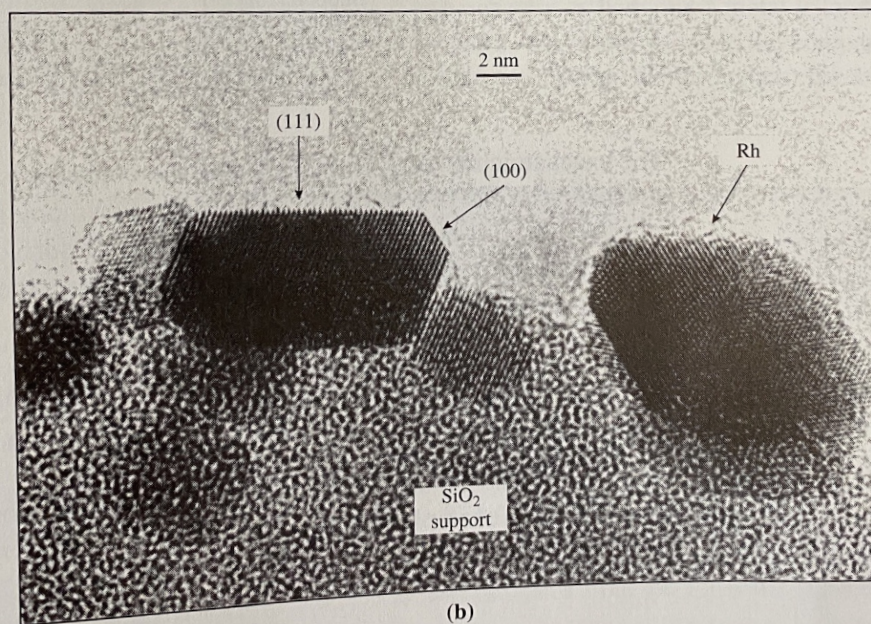
EXACT  
SURFACE  
STRUCTURE  
MATTERS



**Figure 5.1.4** | Schematic representation of a single crystal surface.



(a)



(b)

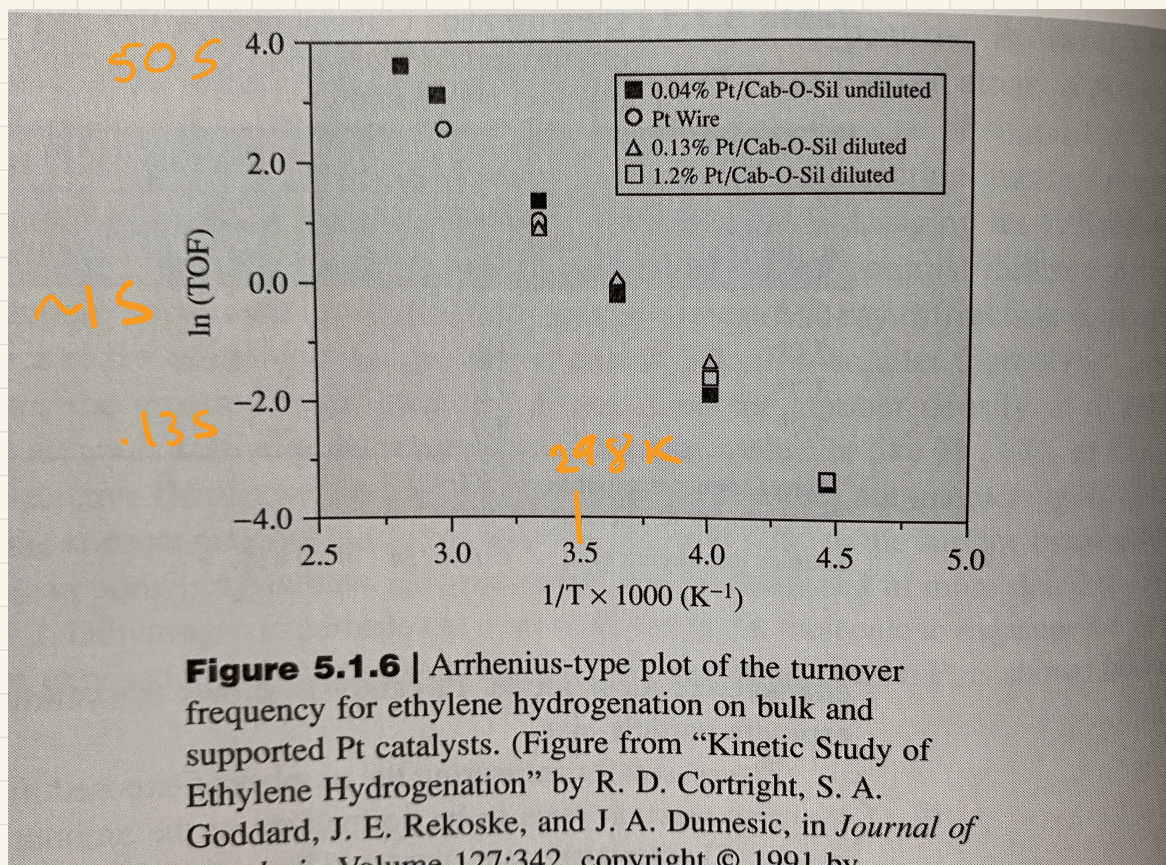
**Figure 5.1.5 |** (a) Rhodium metal particles supported on silica carrier. (b) High-resolution electron micrograph shows how small supported Rh crystallites expose low-index faces. (Top photo courtesy of A. K. Datye. Bottom photo from "Modeling of heterogeneous catalysts using ... A. K. Datye in *Topics in Catalysis*, vol. 13:121 ...)

IF WE CAN STUDY REACTIONS  
AT THIS SCALE, THE  
RATE CAN BE GIVEN AS

$$r_T = \frac{1}{S} \frac{dm}{dt}$$

NUMBER OF  
ACTIVE SITES

TURNOVER  
FREQUENCY



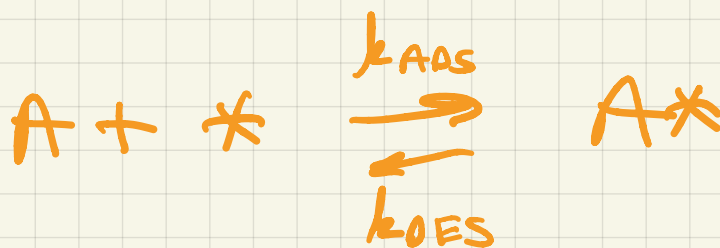
THE CATALYST IS  
A SOLID SURFACE

THE REACTANT IS OFTEN  
A GAS, COULD BE A LIQUID  
IN A SOLVENT, BUT IN  
EITHER CASE A NECESSARY  
STEP IS ADSORPTION ONTO  
THE SURFACE

THE ADSORPTION PROBABLY  
HAS TO BE TO A SPECIFIC  
"SITE"

HENCE WE NEED NOTATION

"\*" ACTIVE SITE





ADSORPTION OF A GAS

ONTO A SURFACE CAN BE

A) PHYSICAL  $\sim$  CONDENSATION

$\sim$  "PHYSISORPTION"  $\Delta H$

OCCURS "ANYWHERE" ON SOLID

B) CHEMICAL  $\sim$   $\Delta H_{RXN}$

"CHEMISORPTION"

OCCURS AT SPECIFIC SITES

# SIMPLEST MODEL FOR ADSORPTION

## "LANGMUIR"

- PHYSICAL ADSORPTION OF
- 1 LAYER COVERAGE
- IDENTICAL SITES THAT DON'T INTERACT
- EQUILIBRIUM BETWEEN GAS  
PHASE AND CONDENSED COMPONENT  
ON SURFACE
- SHOWS HOW TEMPERATURE  
AFFECTS ADSORBED  
AMOUNT
- OFTEN WORKS WHEN YOU  
MIGHT NOT EXPECT....

BUT!!

- PERILS IN STRETCHING TOO  
FAR!!

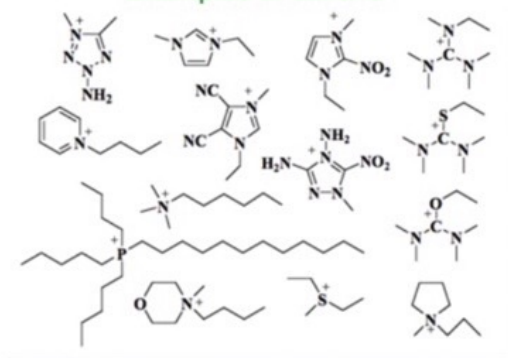
WE HAVE FOUND THAT  
 CHEMICAL COMPLEXATION OF  
 GASEOUS  $\text{CO}_2$  WITH 'DESIGNER'  
 IONIC LIQUIDS FOLLOWS  
 LANGMUIR

## Technology Fundamentals

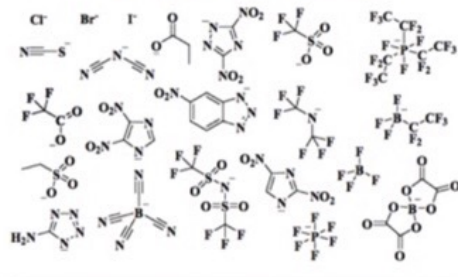
- Ionic liquids are pure salts that are liquid around ambient temperature
  - Not simple salts like alkali halides
- Many favorable properties
  - Nonvolatile
  - Anhydrous
  - High thermal stability
  - Huge chemical diversity
  - High intrinsic  $\text{CO}_2$  solubility and selectivity



Examples of cations

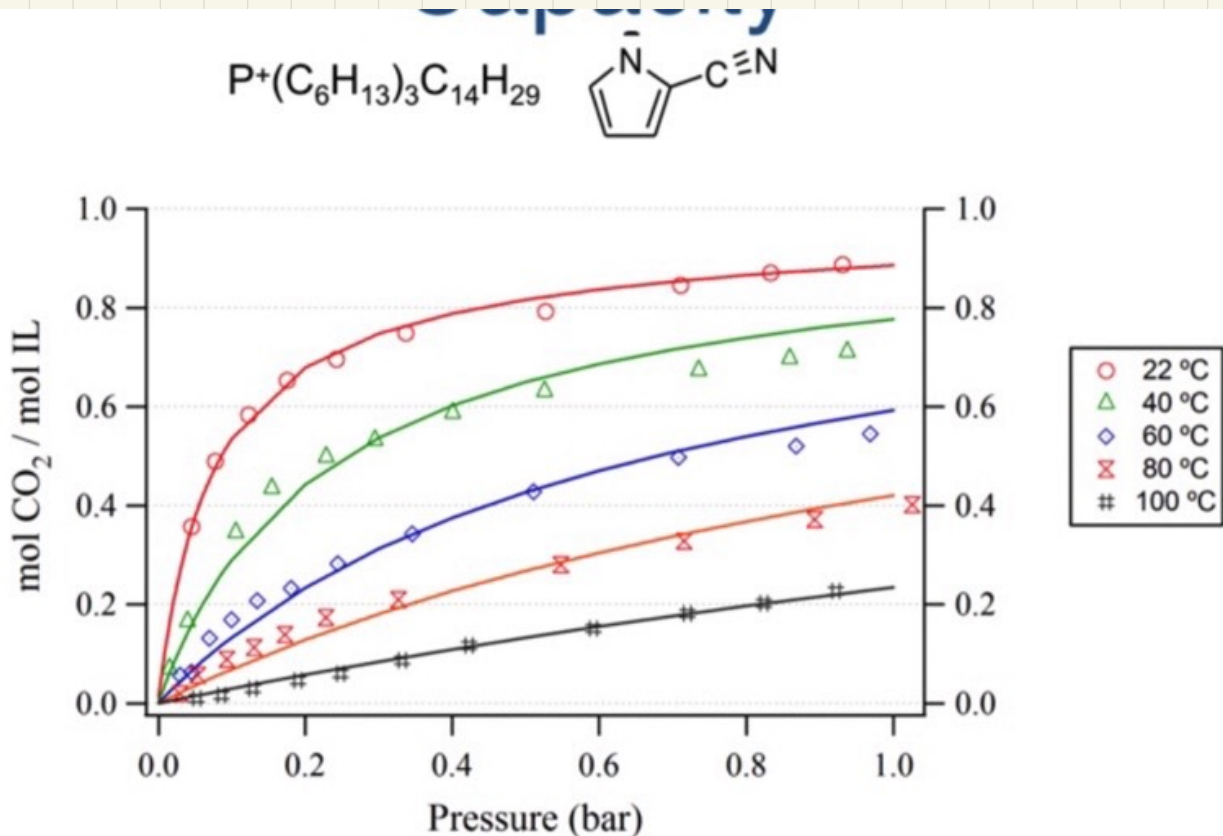
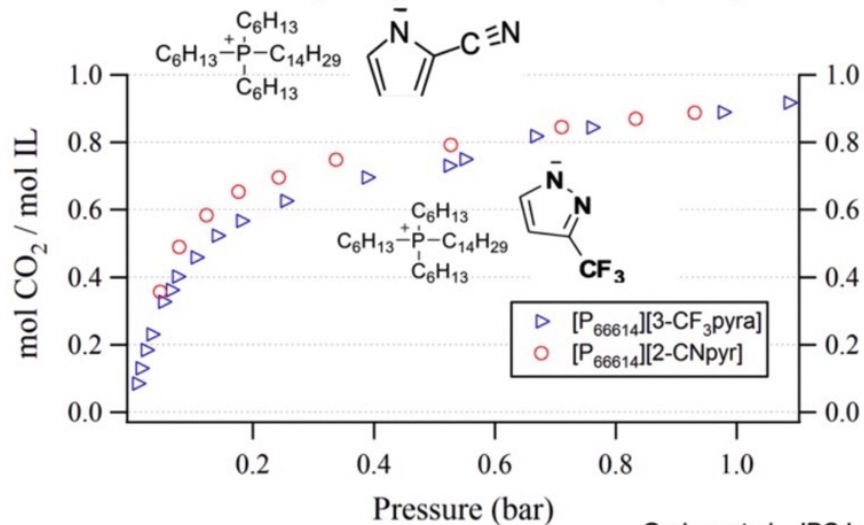


Examples of anions

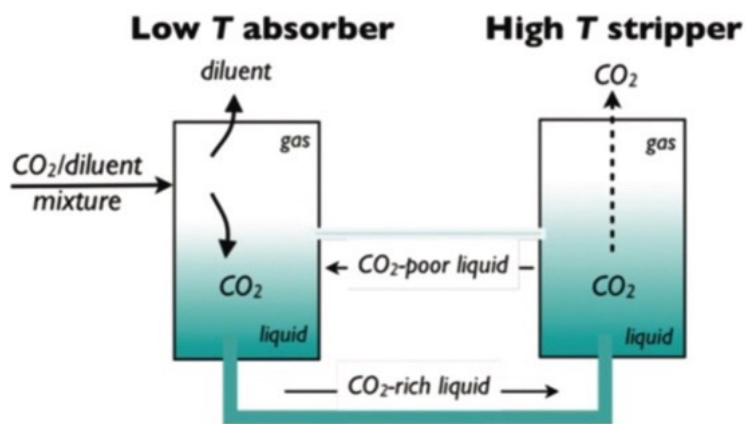
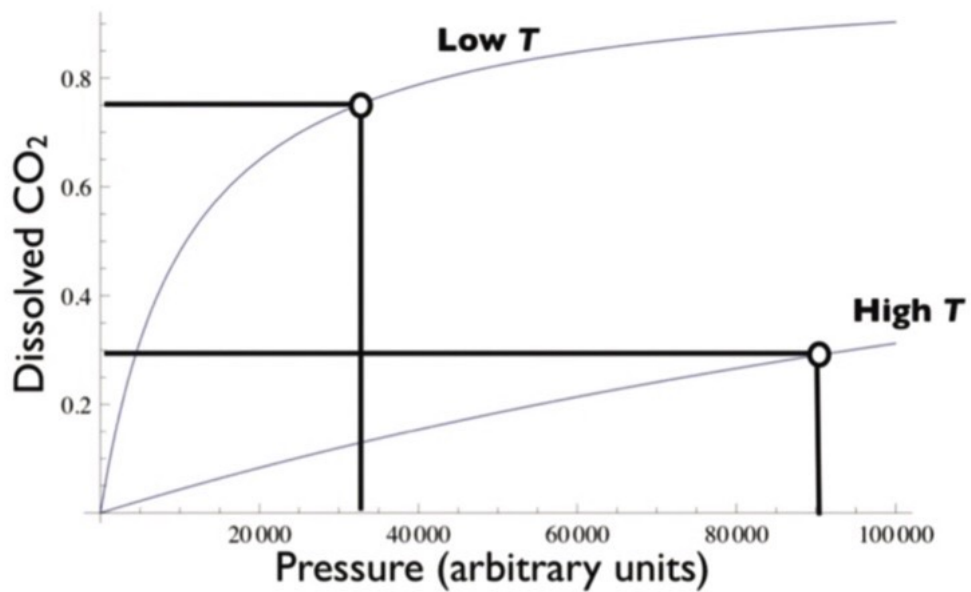


# AHA – aprotic heterocyclic anions

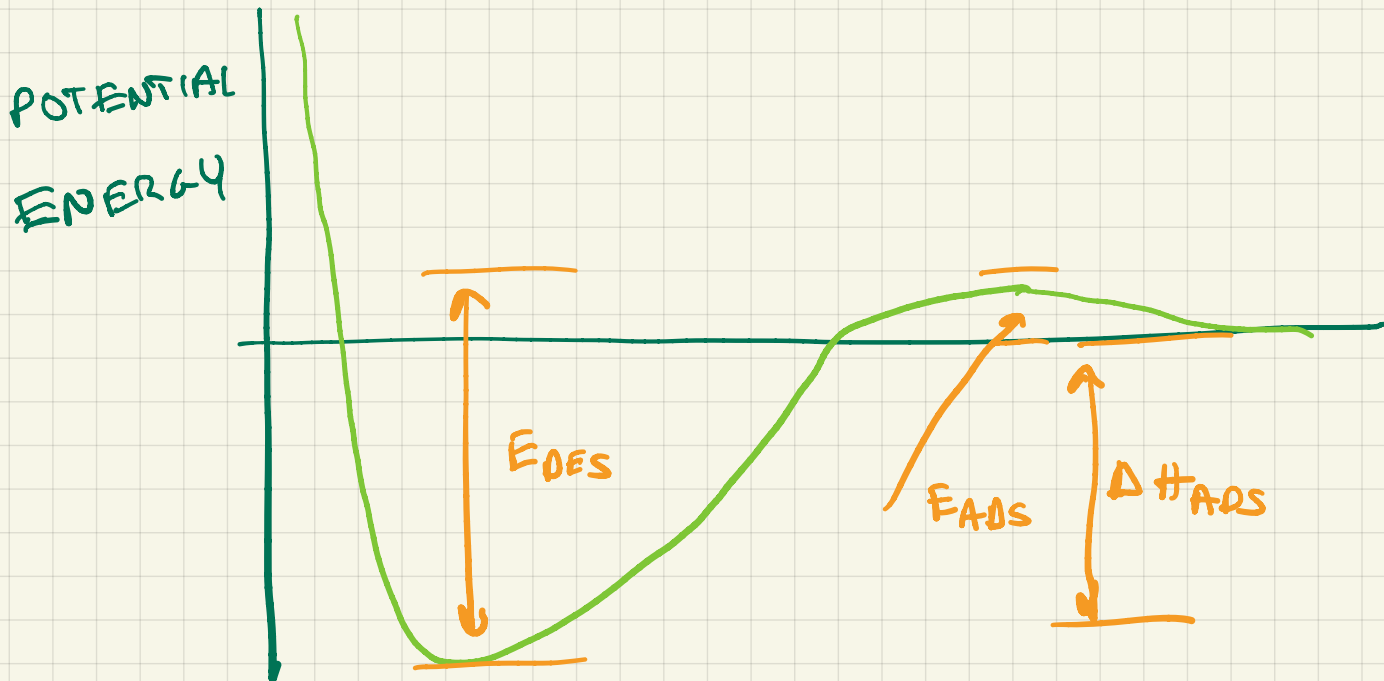
- Retain amine in ring structure
- Further reduce free hydrogens to reduce hydrogen bonding



Experimental confirmation, Gurkan et al.:  
approaches 1:1 IL to CO<sub>2</sub> binding ratio



# ENERGY DIAGRAM FOR ADSORPTION



THIS IS AN EQUILIBRIUM PROCESS  
BUT DERIVATION IS SIMPLEST  
IN TERMS OF RATES,

RATE OF ADSORPTION

=

RATE OF DESORPTION

$S = *$

$$r_{AD} = k_{AD} P_A [S]$$

↑ GAS PRESSURE

↑ CONCENTRATION OF SURFACE SITES

$$r_D = k_D [A_{AD}]$$

$$k_{AD} P_A [S] = k_D [A_{AD}]$$

RATE OF ADSORPTION  
= RATE OF DESORPTION

$$\frac{[A_{AD}]}{P_A [S]} = \frac{k_{AD}}{k_D} = K_{EQ}^A$$

$$[S_0] = \frac{S_0}{a}$$

↑ TOTAL SITES

← AREA

$$[S_0] = [S] + [A_{AD}]$$

$$[S_0] = \frac{[A_{AD}]}{K_{EQ}^A P_A} + [A_{AD}] = \frac{1 + K_{EQ}^A P_A}{K_{EQ}^A P_A} [A_{AD}]$$

$$\theta_A = \frac{[A_{AD}]}{[S_0]}$$

FRACTIONAL COVERAGE

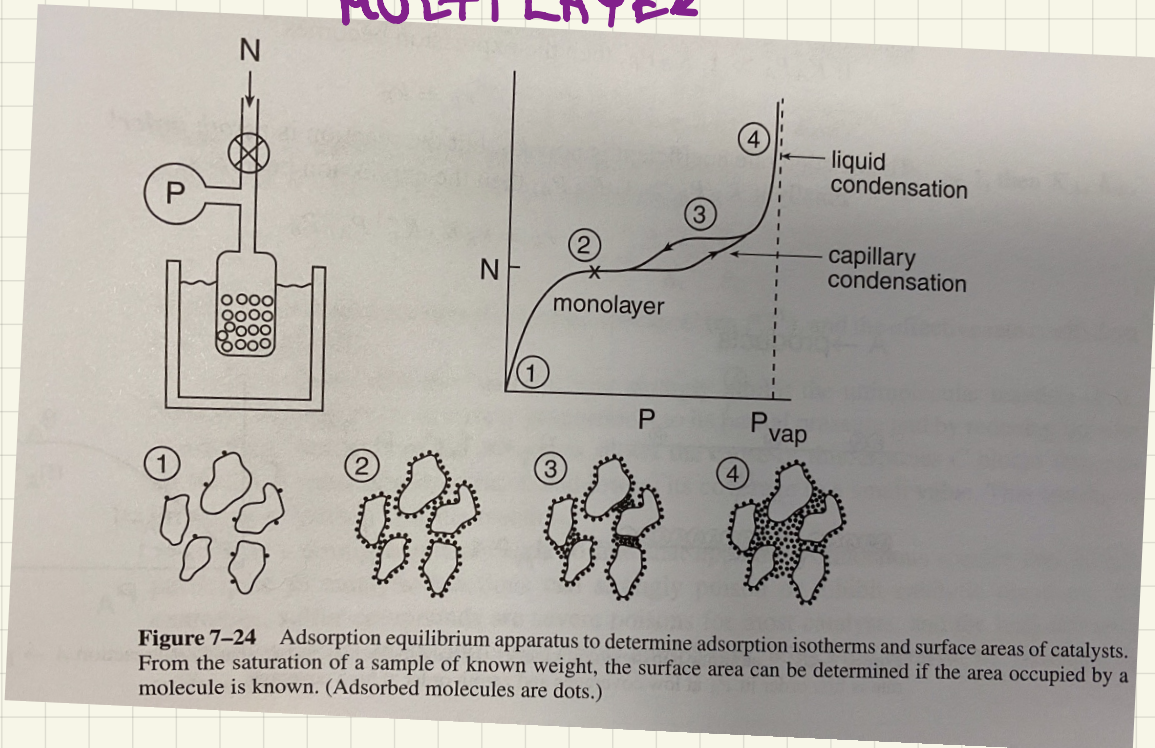
$$\theta_A = \frac{K_{EQ}^A P_A}{1 + K_{EQ}^A P_A}$$





# MORE GENERAL ADSORPTION MODELS EXIST

## B.E.T. BRUNAUER, ENNET, TELLER MULTI LAYER



FROM L. SCHMIDT THE ENGINEERING OF CHEMICAL REACTIONS

$$\frac{P}{V_{\text{ADS}}(P_0 - P)} = \frac{1}{C V_m} + \frac{C-1}{C V_m} \frac{P}{P_0}$$

VOLUME OF GAS ADSORBED (under  $V_{\text{ADS}}$ )  
 GAS PRESSURE (under  $P$ )  
 SAT. PRESS (under  $P_0$ )  
 VOLUME OF GAS THAT GIVES A MONOLAYER (under  $V_m$ )  
 FITTED CONSTANT (under  $C$ )

GET  $C, V_m$  FROM FIT OF DATA



NUMBER OF MOLECULES

$$N = 12$$

$$\alpha = \text{[dashed orange box]}$$

AREA MOLECULE

KNOWN VALUE

$$S_g = N \alpha$$

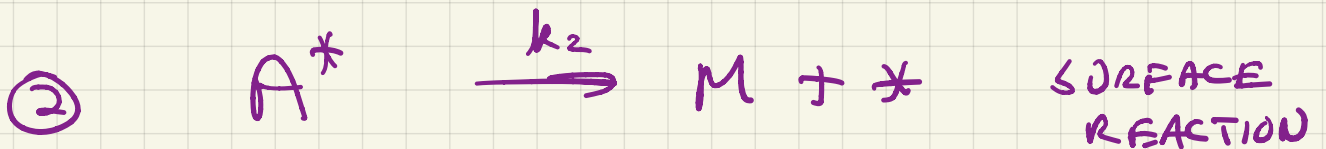
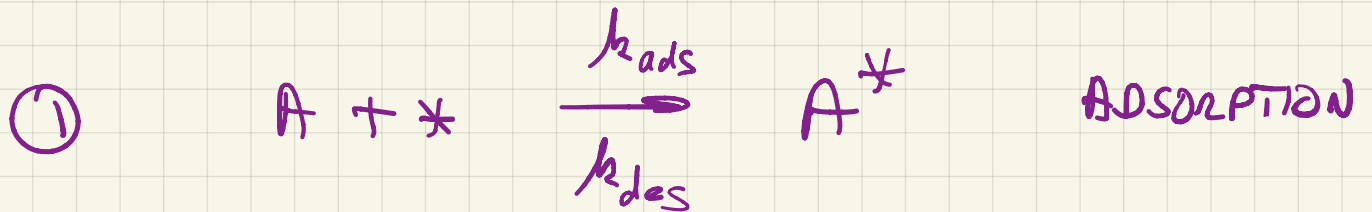
$$N = \frac{V_m N_0}{V}$$

V

STANDARD MOLAR VOLUME OF GAS

# TYPICAL DERIVATION OF RATE EXPRESSION

---



THE RATE MUST BE:  $r = k_2 [A^*]$

WE NEED TO GET  $A^*$  THUS

WE NEED  $* \rightleftharpoons A^*$

$$[*]_0 = [A^*] + [*]$$

USE STEADY STATE!

$$\frac{dA^*}{dt} = 0 = k_{ads} [A][*] - k_{des} [A^*] - k_2 [A^*]$$

$$[X]_0 = [A^*] + [X]$$

$$[X] = [X]_0 - [A^*]$$

$$0 = k_{ads} [A] [X] - k_{des} [A^*] - k_2 [A^*]$$

SOLVE FOR  $[A^*]$

$$[A^*] = \frac{k_{ads} [A] [X]_0}{k_2 + k_{ads} [A] + k_{des}}$$

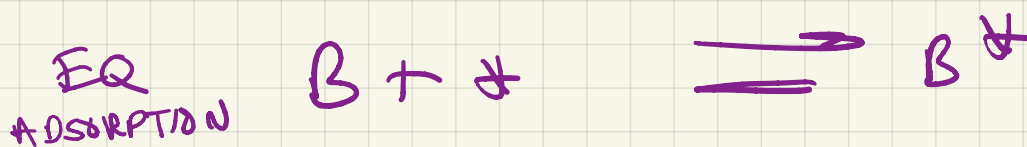
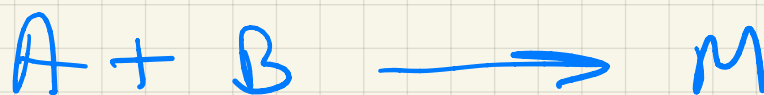
$$= \frac{\frac{k_{ads}}{k_{des}} [A] [X]_0}{1 + \frac{k_2}{k_{des}} + \frac{k_{ads}}{k_{des}} [A]}$$

$$\frac{k_{ads}}{k_{des}} = K_{ads}$$

$$\therefore \Lambda = \frac{k_2 K_{ads} [A] [X]_0}{1 + K_{ads} [A] + \frac{k_2}{k_{des}}}$$

# CONSIDER A SLIGHTLY MORE COMPLEX CASE

---



$$\text{RATE} \rightarrow k_2 A^* B^*$$

BUT FOR A SURFACE REACTION WE KNOW THAT EQ ADSORPTION STEP GIVES A FRACTIONAL COVERAGE SO IT IS CONVENIENT TO WRITE:

$$\text{RATE} = k_3 [*_]_0 \frac{A^*}{[*_]_0} \frac{B^*}{[*_]_0}$$

$$= k_3 [*_]_0 \theta_A \theta_B$$

WHERE  $k_3 = k_2 [*_]_0$

AND  $\theta_A = \frac{K_{adsA} [A]}{1 + K_{adsA} [A] + K_{adsB} [B]}$

$$\theta_B = \frac{K_{adsB} [B]}{1 + K_{adsA} [A] + K_{adsB} [B]}$$

$$r = \frac{K_3 K_{adsA} K_{adsB} [X]_0 [A][B]}{(1 + K_{adsA}[A] + K_{adsB}[B])^2}$$

2 X'S ARE INVOLVED