

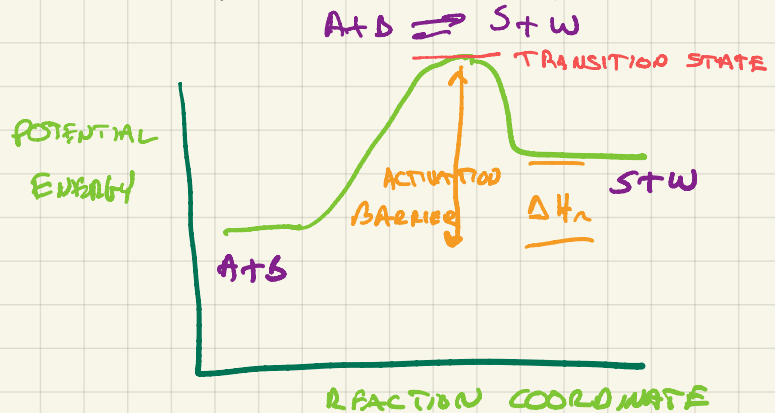
CBE 40455

8/24/20

## REVIEW

$$k = A \exp\left(\frac{E}{RT}\right)$$

### "TRANSITION STATE THEORY"



GENERAL RELATION!

$$\lambda = \left(\frac{\bar{h}T}{h}\right) \exp\left[\frac{\Delta S^\ddagger}{R}\right] \exp\left[\frac{-\Delta H^\ddagger}{RT}\right] C_A C_B$$

$$\bar{A} \hat{=} \frac{\bar{h}T}{h} \hat{=} 10^{13} / s$$

COLLISION FREQUENCY  
FOR NORMALIZED  
BOLTZMAN DISTRIBUTION  
OF MOLECULES

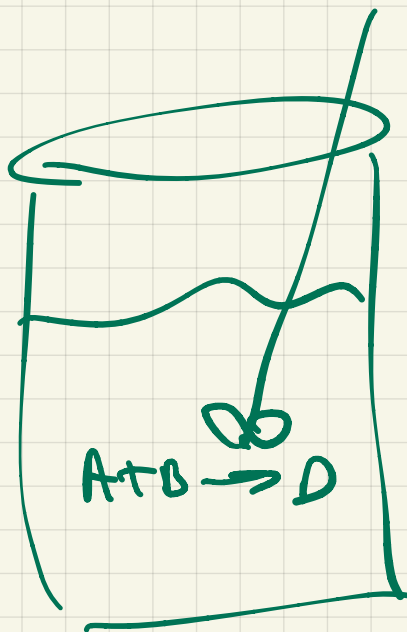
## TODAY

ANALYSIS OF  
DIFFERENT REACTOR  
CONFIGURATIONS . .

# CHAPTER 3

HOW DO WE GET KINETIC DATA ?

IN A LAB, YOU USUALLY  
USE A BATCH OR  
SEMI BATCH REACTOR



BATCH

FEED IN  
B



SEMI BATCH

USED TO  
CAREFULLY  
CONTROL  
CONCENTRATION  
OF 2ND  
REACTANT,  
(PERHAPS  
BECAUSE OF  
SELECTIVITY  
ISSUES)

# ANALYSIS OF A BATCH REACTOR

(MOLES)

## MASS BALANCE

SPECIES  
 $i$

RATE OF  
CHANGE OF  
MOLES OF  
 $i$  IN REACTOR

=

FLOW RATE  
OF  $i$   
INTO  
REACTOR

- FLOW  
RATE  
OF  $i$   
OUT OF  
REACTOR

+ RATE AT  
WHICH  
 $i$  IS PRODUCED/CONSUMED  
BY REACTION

FIRST  
CONSIDER  
A  
BATCH  
REACTOR

THUS IN TERMS OF MOLES...

REACTION RATE  
VOLUME

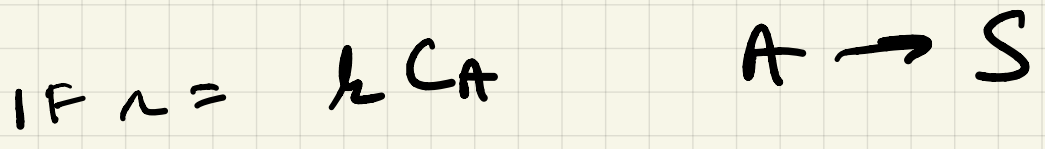
$$\frac{dn_i}{dt} = 0 - 0 + \nu_i r V$$

Annotations:  
-  $\nu_i$ : STOICHIOMETRIC COEFFICIENT  
-  $r$ : REACTION RATE  
-  $V$ : VOLUME

GENERALLY AN INITIAL  
VALUE PROBLEM

COULD ALSO WRITE

$$\frac{dV C_i}{dt} = \nu_i r V$$



$$\frac{dV C_A}{dt} = -k C_A V$$

IF  $V = \text{CONST}$

~~$V \frac{dC_A}{dt} = -k C_A V$~~

COULD ALSO WRITE:

$$M_i^0 \frac{df_i}{dt} = -v_i n V \quad f_i(t=0) = 0$$

SUPPOSE  $A + B \rightarrow S$

$$r = k C_A C_B$$

$$C_{A0} \neq C_{B0}$$

$$dC_A = dC_B$$

$$C_{A0} - C_A = C_{B0} - C_B$$

$V = \text{CONST}$

$$C_B = (C_{B0} - C_{A0}) + C_A$$

$$\frac{dC_A}{dt} = -k C_A C_B$$

$$\frac{dC_A}{dt} = -k C_A (C_{B0} - C_{A0} + C_A)$$

$$\frac{dC_A}{C_A (C_A - (C_{A0} - C_{B0}))} = -k dt \quad \text{CORRECTIONS}$$

$$\frac{dC_A}{C_A (C_A - (C_{A0} - C_{B0}))} = -k dt$$

~~$$\ln \left( \frac{C_{A0} (C_A(t) - (C_{A0} - C_{B0}))}{C_{A0} - C_{B0}} \right) = kt$$~~

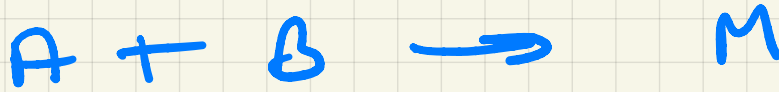
$$\frac{\ln \left( \frac{C_A - C_{A0} + C_{B0}}{C_A} \right)}{(C_{A0} - C_{B0})} = -kt$$

$$\frac{C_A}{C_{A0}} = \frac{(C_{A0} - C_{B0})}{C_{A0} - \exp((C_{A0} - C_{B0})kt)}$$

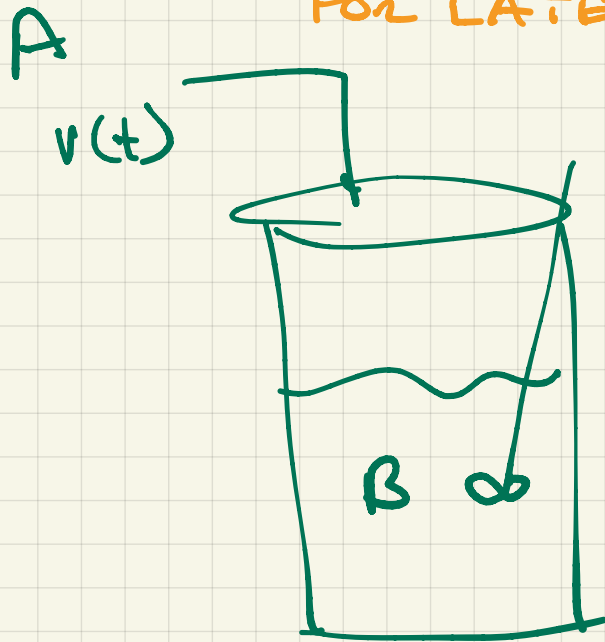
WE WOULD USE THIS  
AS EXPECTED!

$C(t)$  DATA  $\rightarrow k$

# NOW CONSIDER A "SEMI-BATCH" REACTOR



SAVE OTHER REACTIONS  
FOR LATER . . .



WOULD ADJUST IF  
NECESSARY

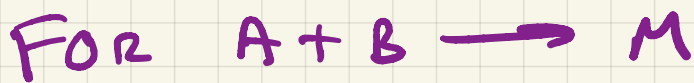
FOR  
COMPONENT  
 $i$

$$\frac{dn_i}{dt} = f(t) C_i^0(t) - r_i(t) V$$

MIGHT  
CHANGE

IF RECIPE  
IS  
COMPLEX





$$r = k C_A C_B \quad C_B^0 \rightarrow \text{INITIAL IN REACTOR}$$

$$\frac{dn_A}{dt} = q C_A^0 - k C_A C_B V$$

$$\frac{dn_B}{dt} = 0 - k C_A C_B V$$

$$V = V_0 + q * t$$

$$k C_A C_B V = k \frac{n_A}{V} \frac{n_B}{V} V$$

$$= \frac{k n_A n_B}{(V_0 + q * t)}$$

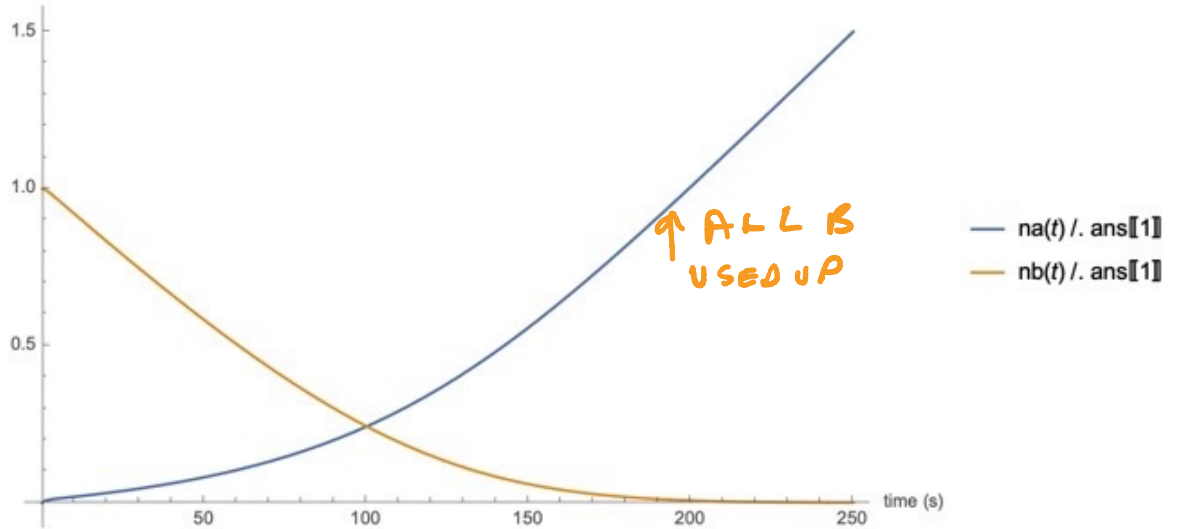
$$\frac{dn_A}{dt} = V^0 C_A^0 - \frac{k n_A n_B}{(V_0 + q * t)}$$

$$\frac{dn_B}{dt} = - \frac{k n_A n_B}{(V_0 + q * t)}$$

# SOLVE NUMERICALLY

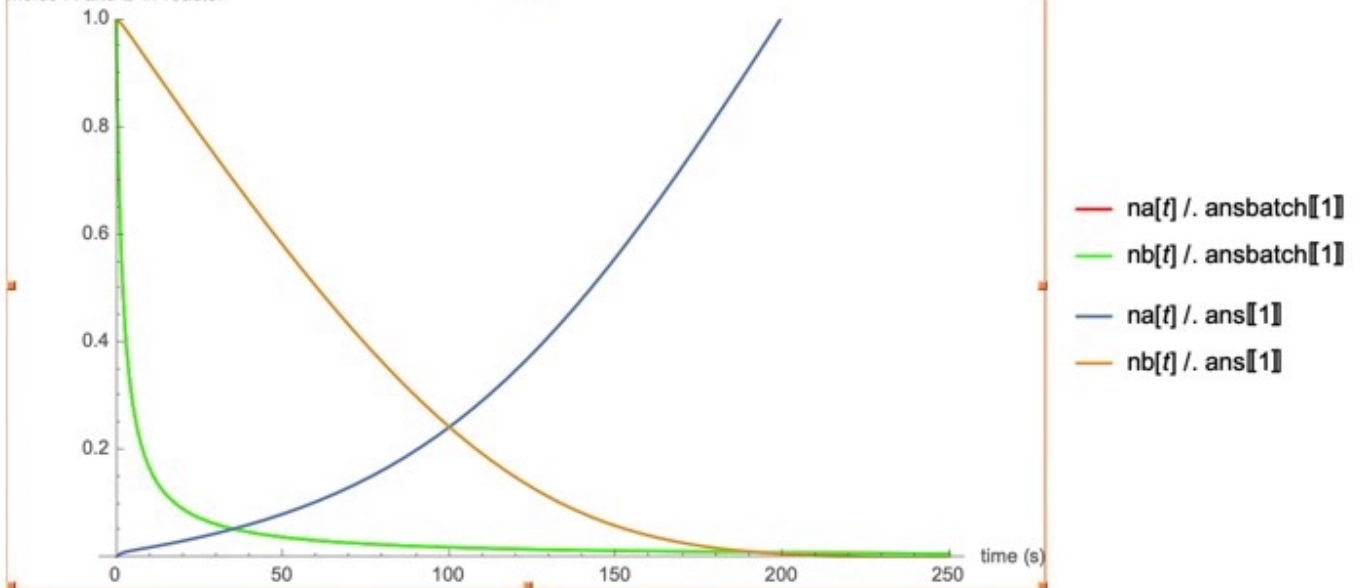
```
Plot[{na[t] /. ans[[1]], nb[t] /. ans[[1]]}, {t, 0, 250},  
AxesLabel -> {"time (s)", "moles A and B in reactor"}, PlotLegends -> "Expressions"]
```

moles A and B in reactor



IF ALL A IS ADDED AT BEGINNING, REACTION IS MUCH FASTER

moles A and B in reactor



IF YOU REALLY WANT TO,  
AN ANALYTICAL SOLUTION IS  
POSSIBLE . . .

analyticalans =

```
FullSimplify[DSolve[{eq1 == 0, eq2 == 0, na[0] == na0, nb[0] == nb0}, {na[t], nb[t]}, t,
  Assumptions -> {V0 > 0, v0 > 0, ca0 > 0, k > 0, na0 >= 0, nb0 > 0, t > 0}]]
```

$$\left\{ \left\{ na[t] \rightarrow \left( e^{-\frac{ca_0 k (t v_0 + V_0)}{v_0}} \right. \right. \right.$$

$$\left. \left( e^{\frac{ca_0 k V_0}{v_0}} nb_0 v_0 (t v_0 + V_0)^{\frac{k(-na_0 + nb_0 + ca_0 V_0)}{v_0}} + (na_0 - nb_0 + ca_0 t v_0) \left( e^{\frac{ca_0 k (t v_0 + V_0)}{v_0}} v_0 V_0^{\frac{k(-na_0 + nb_0 + ca_0 V_0)}{v_0}} + \right. \right. \right.$$

$$\left. \left. e^{ca_0 k \left( t + \frac{2V_0}{v_0} \right)} k nb_0 \left( \frac{v_0}{ca_0 k} \right)^{\frac{k(-na_0 + nb_0 + ca_0 V_0)}{v_0}} \left( \text{Gamma} \left[ \frac{k(-na_0 + nb_0 + ca_0 V_0)}{v_0}, \frac{ca_0 k V_0}{v_0} \right] - \right. \right.$$

$$\left. \left. \text{Gamma} \left[ \frac{k(-na_0 + nb_0 + ca_0 V_0)}{v_0}, \frac{ca_0 k (t v_0 + V_0)}{v_0} \right] \right) \right) \right) \right) /$$

$$\left( v_0 V_0^{\frac{k(-na_0 + nb_0 + ca_0 V_0)}{v_0}} + e^{\frac{ca_0 k V_0}{v_0}} k nb_0 \left( \frac{v_0}{ca_0 k} \right)^{\frac{k(-na_0 + nb_0 + ca_0 V_0)}{v_0}} \left( \text{Gamma} \left[ \frac{k(-na_0 + nb_0 + ca_0 V_0)}{v_0}, \frac{ca_0 k V_0}{v_0} \right] - \right. \right.$$

$$\left. \left. \text{Gamma} \left[ \frac{k(-na_0 + nb_0 + ca_0 V_0)}{v_0}, \frac{ca_0 k (t v_0 + V_0)}{v_0} \right] \right) \right),$$

$$nb[t] \rightarrow \left( e^{-ca_0 k t} nb_0 v_0 (t v_0 + V_0)^{\frac{k(-na_0 + nb_0 + ca_0 V_0)}{v_0}} \right) / \left( v_0 V_0^{\frac{k(-na_0 + nb_0 + ca_0 V_0)}{v_0}} + e^{\frac{ca_0 k V_0}{v_0}} k nb_0 \left( \frac{v_0}{ca_0 k} \right)^{\frac{k(-na_0 + nb_0 + ca_0 V_0)}{v_0}} \right.$$

$$\left. \left( \text{Gamma} \left[ \frac{k(-na_0 + nb_0 + ca_0 V_0)}{v_0}, \frac{ca_0 k V_0}{v_0} \right] - \text{Gamma} \left[ \frac{k(-na_0 + nb_0 + ca_0 V_0)}{v_0}, \frac{ca_0 k (t v_0 + V_0)}{v_0} \right] \right) \right) \right\}$$

$$\frac{dn_B}{dt} = -k C_A C_B V$$

$$\frac{dV C_B}{dt} = -k C_A C_B V$$

$$C_B \frac{dV}{dt} + V \frac{dC_B}{dt} = -k C_A C_B V$$

$$V = V_0 + q t$$

$$\frac{dV}{dt} = q$$

$$V \frac{dC_B}{dt} = -k C_A C_B V - C_B q$$

$$\frac{dC_B}{dt} = -C_B \frac{q}{V} - k C_A C_B$$

$$\frac{dC_B}{dt} = -C_B \frac{q}{V} - k C_A C_B$$

$$\frac{dV C_A}{dt} = q C_A^0 - k C_A C_B V$$

$$V \frac{dC_A}{dt} + C_A q = q C_A^0 - k C_A C_B V$$

$$\frac{dC_A}{dt} = \frac{q(C_A^0 - C_A)}{V} - k C_A C_B$$

SUBTRACT EQ'S

$$\frac{dC_B}{dt} - \frac{dC_A}{dt} = -C_B \frac{q}{V} - C_A^0 \frac{q}{V} + C_A \frac{q}{V}$$

$$\frac{dC_A}{dt} - \frac{dC_B}{dt} = (-C_B + C_A - C_A^0) \frac{q}{V}$$

BUT WE CAN NONDIMENSIONALIZE

$$X_B = \frac{C_B}{C_{A0}} \quad \tau = \frac{V}{q}$$

$$X_A = \frac{C_A}{C_{A0}} \quad \tau = \frac{t}{\tau}$$

$$\frac{dC_B}{dt} = -C_B \frac{q}{V} - k C_A C_B$$

$$C_{A0} \frac{dX_B}{dt} = \frac{C_{A0} X_B}{\tau} - k C_{A0}^2 X_A X_B$$

$$\frac{dX_B}{d\tau} = X_B - (k C_{A0} \tau) X_A X_B$$

$$\frac{dX_B}{d\tau} = X_B - Da X_A X_B$$

$$\frac{dC_A}{dt} = q \frac{(C_A^0 - C_A)}{V} - k C_A C_B$$

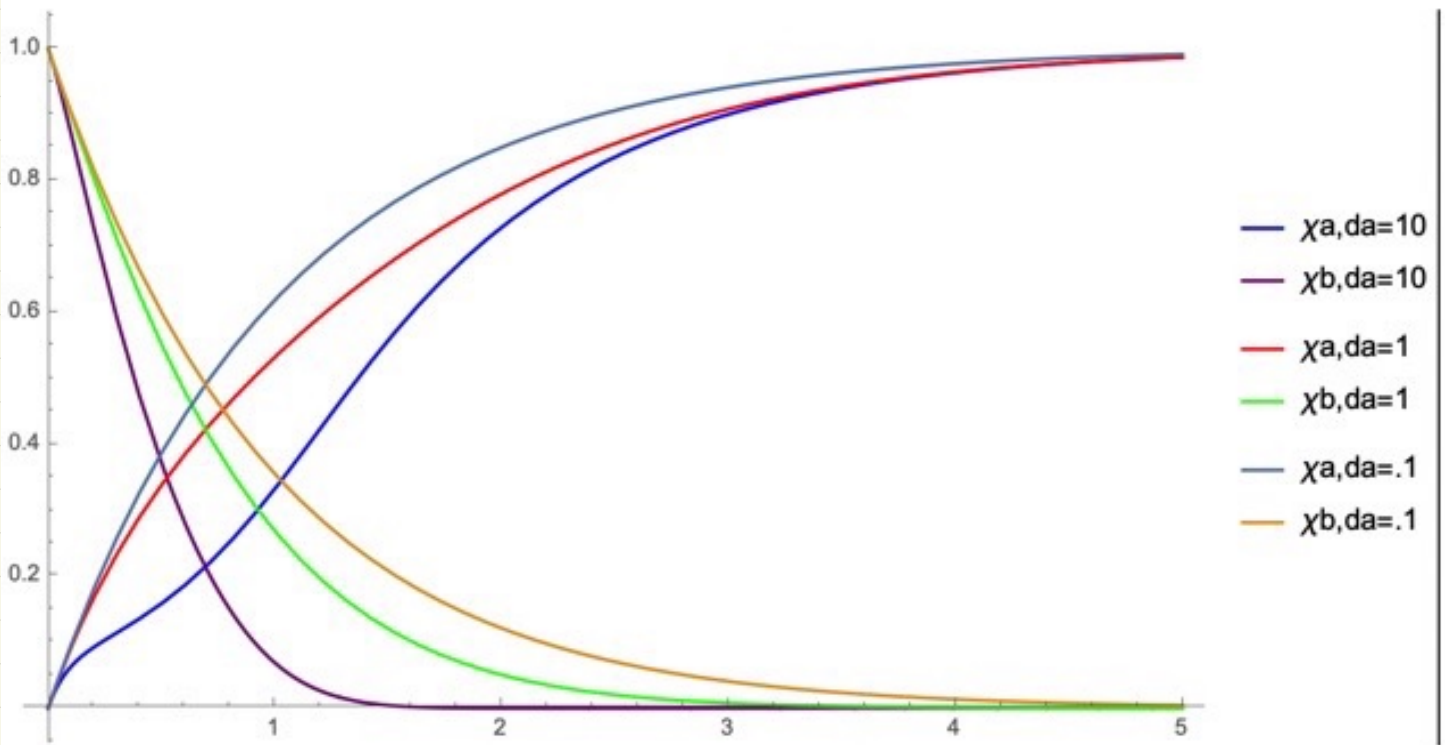
$$C_{A0} \frac{dX_A}{dt} = \frac{(1 - X_A) C_{A0}}{\tau} - k C_{A0}^2 X_A X_B$$

$$\begin{cases} \frac{dX_A}{d\tau} = (1 - X_A) - Da X_A X_B \\ \frac{dX_B}{d\tau} = -X_B - Da X_A X_B \end{cases}$$

WE CAN MAKE THESE

SIMPLER TO LOOK AT !!

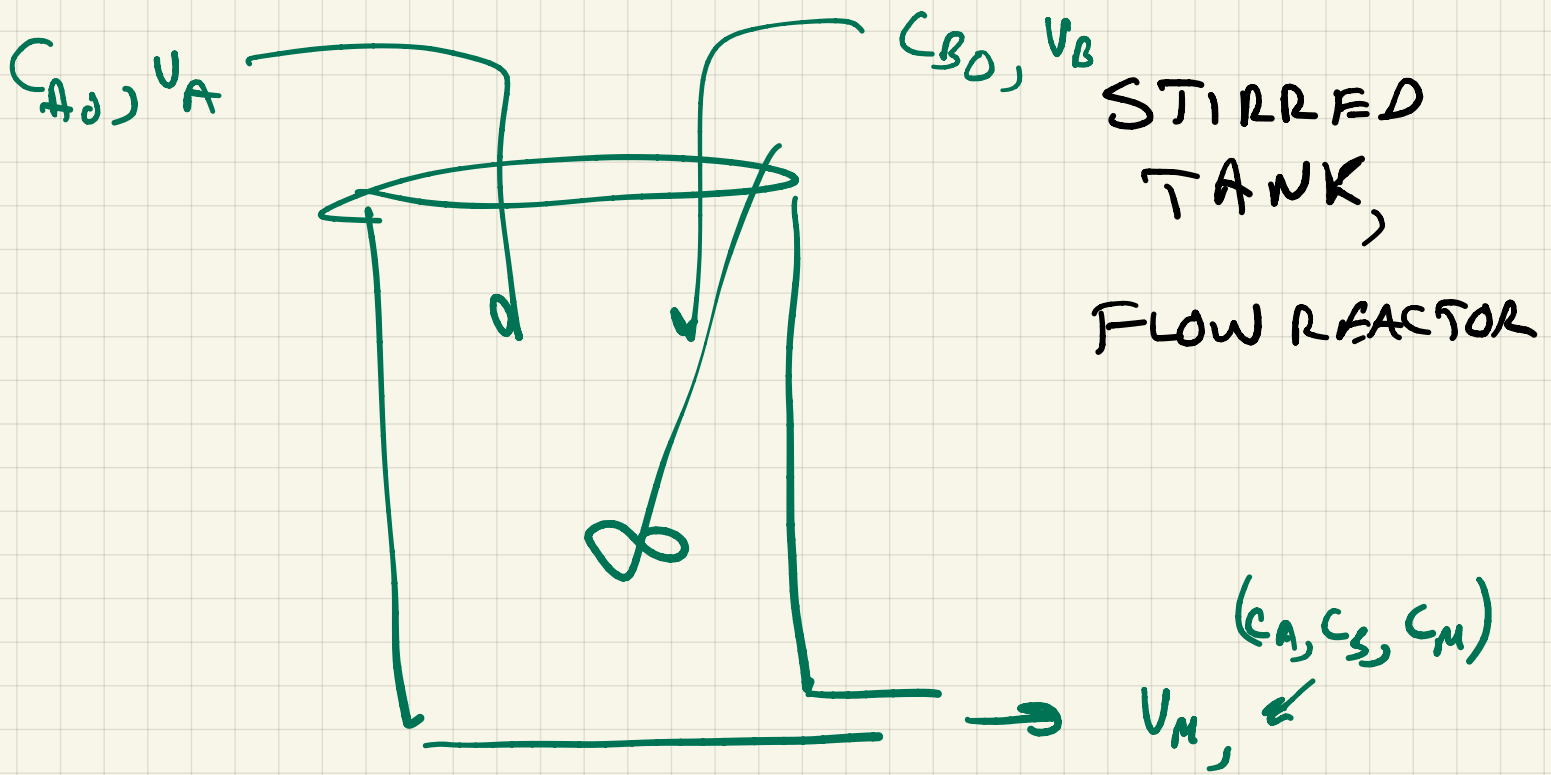
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AS  $Da \uparrow$  FASTER REACTION

BUT THIS IS MITIGATED  
SOMEWHAT BY "A"  
GETTING USED UP





## GENERAL EQUATIONS!

OVERALL  
MASS  
BALANCE

$$\frac{d\rho V}{dt} = \rho_A q_A + \rho_B q_B - \rho q$$

$$q = q_A + q_B$$

CHANGE IN  
DENSITY IS  
NOT AN ISSUE  
FOR LIQUIDS  
IF NO  $\Delta V_{mix}$

$$\frac{dV}{dt} = q_A + q_B - q$$

COULD BE  
FILLING UP.

$$\text{COMPONENT A} \quad \frac{d}{dt} V C_A = q_A C_{A0} - q C_A + v_A \tau V$$

$$\text{COMPONENT B} \quad \frac{d}{dt} V C_B = q_B C_{B0} - q C_B + v_B \tau V$$

$$\text{COMPONENT M} \quad \frac{d}{dt} V C_M = 0 - q C_M + v_M \tau V$$

STANDARD ASSUMPTIONS FOR  
STEADY-STATE OPERATION,

$$\frac{d}{dt} ( ) = 0$$

JUST LOOK AT COMPONENT  
A.  $\rightarrow$   $A+B \rightarrow 2M$

$$0 = q_A C_{A0} - q C_A + v_A \tau V$$

$$C_A = \frac{q_A C_{A0}}{q} + v_A \tau \frac{V}{q}$$

OR

$$-v_A \tau = \frac{q_A C_{A0} - q C_A}{V}$$

WE CAN WRITE: ↙  $\frac{\text{MOLES}}{\text{TIME}}$

$$-v_A \tau = \frac{F_{A0} - F_A}{V}$$

WE COULD ALSO WRITE:

$$f = \frac{F_{A0} - F_A}{F_{A0}}$$

WHICH GIVES:

$$-v_A \tau = \frac{F_{A0}}{V} f_A$$

MOST  
USEFUL  
FOR  
LIMITING  
REACTANT.