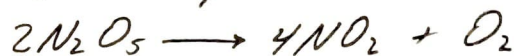
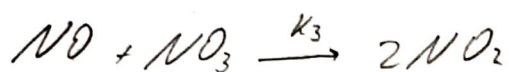
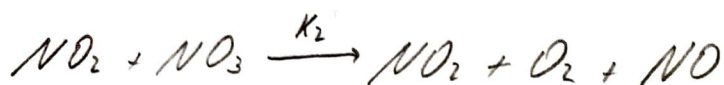
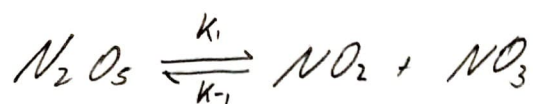


Problem #1

N_2O_5 Decomposition



Experimentally: $r = \frac{d[O_2]}{dt} = k[N_2O_5]$



Need to solve for intermediates: NO_3 and NO

$$\frac{d[NO_3]}{dt} = k_1[N_2O_5] - k_{-1}[NO_2][NO_3] - k_2[NO_2][NO_3] - k_3[NO][NO_3]$$

$$\frac{d[NO]}{dt} = k_2[NO_2][NO_3] - k_3[NO][NO_3]$$

Steady-State

$$\frac{d[NO]}{dt} = 0 \Rightarrow k_2[NO_2][NO_3] = k_3[NO][NO_3]$$

$$[NO_2] = \frac{k_3}{k_2} [NO]$$

Substitute $[NO_2]$ in $\frac{d[NO_3]}{dt} = 0$

$$0 = k_1[N_2O_5] - k_{-1} \frac{k_3}{k_2} [NO][NO_3] - \frac{k_2 k_3}{k_2} [NO][NO_3] - k_3 [NO][NO_3]$$

$$0 = k_1[N_2O_5] - [NO][NO_3] \left[\frac{k_{-1}k_3}{k_2} + 2k_3 \right]$$

$$k_1[N_2O_5] = \left[\frac{k_{-1}k_3}{k_2} + 2k_3 \right] [NO][NO_3] \Rightarrow$$

$$[NO_3] = \frac{k_1}{\left[\frac{k_{-1}k_3}{k_2} + 2k_3\right]} \frac{[N_2O_5]}{[NO]}$$

$$\frac{d[O_2]}{dt} = k_2 [NO_3] [NO]$$

$$\frac{d[O_2]}{dt} = k_2 \left(\frac{k_1}{\frac{k_{-1}k_3}{k_2} + 2k_3} \frac{[N_2O_5]}{[NO]} \right) \left(\frac{k_3}{k_2} [NO] \right) = \frac{k_1 k_3}{\frac{k_{-1}k_3}{k_2} + 2k_3} [N_2O_5]$$

$$\frac{d[O_2]}{dt} = \frac{k_1 k_3}{k_3 \left(\frac{k_{-1}}{k_2} + 2 \right)} [N_2O_5] = \frac{k_1}{\frac{k_{-1}}{k_2} + 2k_2} [N_2O_5]$$

$$\frac{d[O_2]}{dt} = \frac{k_1 k_2}{k_{-1} + 2k_2} [N_2O_5]$$

$$K = \frac{k_1 k_2}{k_{-1} + 2k_2}$$

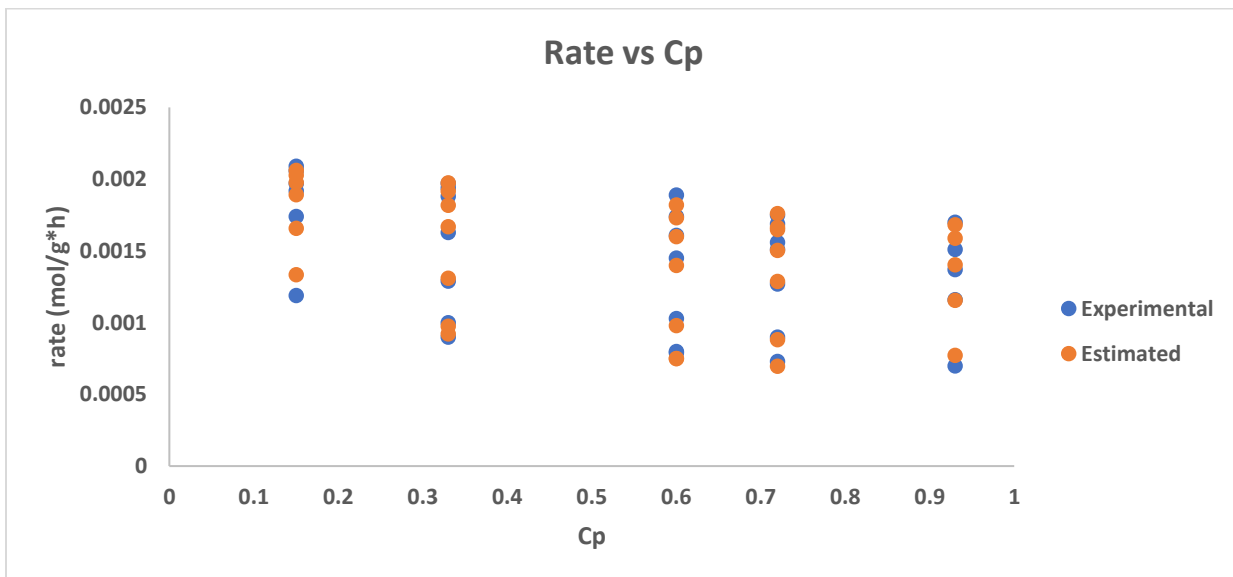
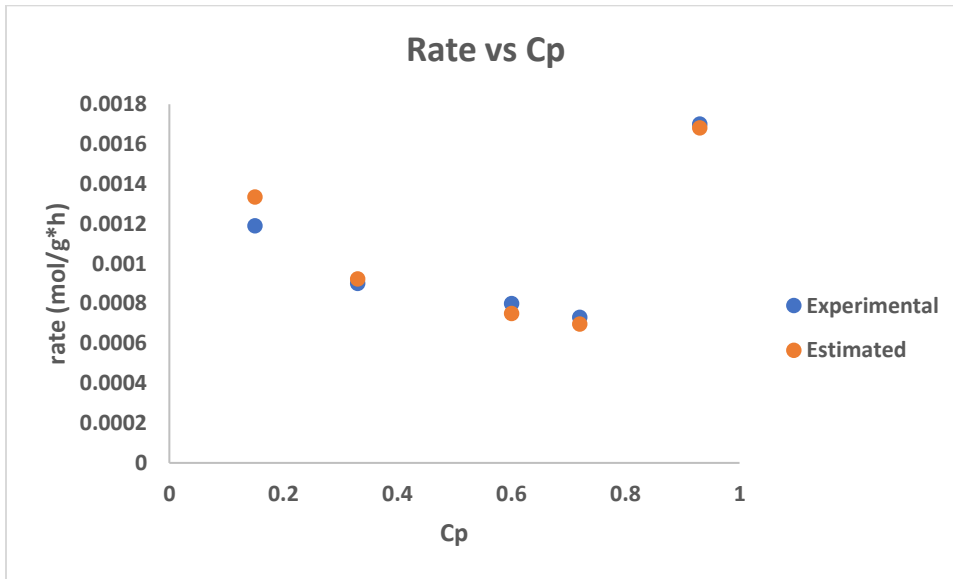
$$\therefore \frac{d[O_2]}{dt} = K [N_2O_5]$$

Problem 2

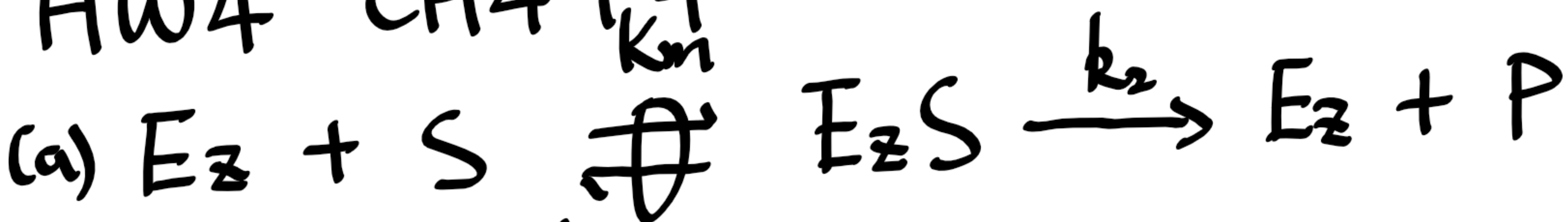
| Cp (mol/L) | Ca (mol/L) | rate (mmol/g*h) | rate (mol/g*h) | Estimated rate (mol/g*h) | Normalized error ^2 |
|---------------|---------------|--------------------|-------------------|-----------------------------|---------------------|
| 0.15 | 0.1 | 1.19 | 0.00119 | 0.001334666 | 0.014778865 |
| 0.15 | 0.2 | 1.74 | 0.00174 | 0.001657764 | 0.002233717 |
| 0.15 | 0.41 | 1.92 | 0.00192 | 0.001892409 | 0.000206511 |
| 0.15 | 0.6 | 1.97 | 0.00197 | 0.001976793 | 1.18909E-05 |
| 0.15 | 0.82 | 2.06 | 0.00206 | 0.002029178 | 0.000223863 |
| 0.15 | 1.04 | 2.09 | 0.00209 | 0.002060683 | 0.000196766 |
| 0.33 | 0.1 | 0.9 | 0.0009 | 0.00092271 | 0.000636694 |
| 0.33 | 0.11 | 1 | 0.001 | 0.00097514 | 0.000618024 |
| 0.33 | 0.2 | 1.29 | 0.00129 | 0.001310144 | 0.000243836 |
| 0.33 | 0.41 | 1.63 | 0.00163 | 0.00166911 | 0.000575692 |
| 0.33 | 0.6 | 1.88 | 0.00188 | 0.001819454 | 0.001037171 |
| 0.33 | 0.81 | 1.94 | 0.00194 | 0.001916007 | 0.000152953 |
| 0.33 | 1.01 | 1.97 | 0.00197 | 0.001975314 | 7.27504E-06 |
| 0.6 | 0.13 | 0.8 | 0.0008 | 0.000750162 | 0.003880994 |
| 0.6 | 0.13 | 0.79 | 0.00079 | 0.000750162 | 0.002542981 |
| 0.6 | 0.2 | 1.03 | 0.00103 | 0.000980812 | 0.00228058 |
| 0.6 | 0.42 | 1.45 | 0.00145 | 0.001399362 | 0.001219609 |
| 0.6 | 0.62 | 1.61 | 0.00161 | 0.001599532 | 4.22717E-05 |
| 0.6 | 0.83 | 1.74 | 0.00174 | 0.001731101 | 2.61558E-05 |
| 0.6 | 1.04 | 1.89 | 0.00189 | 0.001820365 | 0.001357463 |
| 0.72 | 0.14 | 0.73 | 0.00073 | 0.000697291 | 0.002007703 |
| 0.72 | 0.2 | 0.9 | 0.0009 | 0.000881236 | 0.000434689 |
| 0.72 | 0.41 | 1.27 | 0.00127 | 0.001286988 | 0.000178935 |
| 0.72 | 0.61 | 1.51 | 0.00151 | 0.001503094 | 2.09166E-05 |
| 0.72 | 0.82 | 1.56 | 0.00156 | 0.001648411 | 0.003211916 |
| 0.72 | 0.85 | 1.69 | 0.00169 | 0.001664913 | 0.000220355 |
| 0.72 | 1.06 | 1.75 | 0.00175 | 0.00176034 | 3.49121E-05 |
| 0.93 | 0.21 | 0.7 | 0.0007 | 0.000772731 | 0.010795461 |
| 0.93 | 0.42 | 1.16 | 0.00116 | 0.001156637 | 8.40442E-06 |
| 0.93 | 0.65 | 1.37 | 0.00137 | 0.00140334 | 0.000592232 |
| 0.93 | 0.93 | 1.51 | 0.00151 | 0.001589766 | 0.002790521 |
| 0.93 | 1.13 | 1.7 | 0.0017 | 0.001681549 | 0.000117799 |
| | | | | | |
| | | | | sum | 0.052687154 |

| | |
|-------------|----------|
| rmax | 0.002321 |
| k1 | 0.000299 |
| k2 | 0.009198 |
| kpi | 0.000665 |

| Cp (mol/L) | rate (mol/g*h) | Estimated rate (mol/g*h) |
|-------------------|-----------------------|---------------------------------|
| 0.15 | 0.00119 | 0.001334666 |
| 0.33 | 0.0009 | 0.00092271 |
| 0.6 | 0.0008 | 0.000750162 |
| 0.72 | 0.00073 | 0.000697291 |
| 0.93 | 0.0017 | 0.001681549 |



HW4 CH4 P4



$$r = k_2 C_{E_z S}$$

$$C_{E_z}^0 = C_{E_z S} + C_{E_z} + C_{E_z I}$$

\therefore Steady-state approximation

$$k_m = \frac{C_{E_z} C_S}{C_{E_z S}}$$

$$k_i = \frac{C_{E_z} C_I}{C_{E_z I}}$$

$$C_{E_z S} = C_S C_{E_z} / k_m \quad C_{E_z I} = C_I C_{E_z}$$

$$\therefore C_{E_z}^0 = C_S C_{E_z} / k_m + C_I C_{E_z} / k_i + C_{E_z}$$

$$C_{E_z} = \frac{C_{E_z}^0}{(1 + C_S / k_m + C_I / k_i)}$$

$$\therefore C_{E_z S} = \frac{k_m C_S C_{E_z}^0}{(1 + C_S / k_m + C_I / k_i)}$$

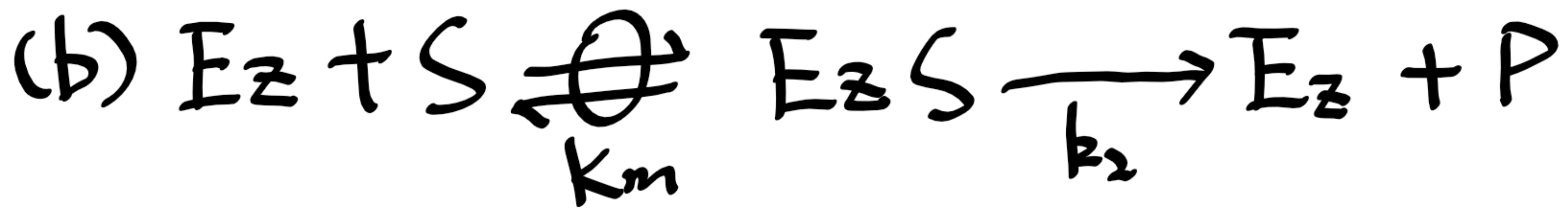
$$r = k_2 C_{E_2} S$$

$$= \frac{k_2 C_s C_{E_2}^0 / K_m}{1 + C_s / K_m + C_i / K_i}$$

$$= \frac{k_2 C_{E_2}^0 C_s}{K_m \left(1 + \frac{C_i}{K_i}\right) + C_s}$$

$$k_2 C_{E_2}^0 = r_{\max}$$

$$\therefore r = \frac{r_{\max} C_s}{K_m \left(1 + \frac{C_i}{K_i}\right) + C_s}$$



$$r = k_2 C_{E_2S}$$

$$C_{E_2}^0 = C_{E_2} + C_{E_2S} + C_{E_2SI}$$

\therefore Steady-State Appx.

$$k_m = \frac{C_{E_2} C_S}{C_{E_2S}} \quad k_i = \frac{C_{E_2S} C_I}{C_{E_2SI}}$$

$$\therefore C_{E_2} = \frac{k_m C_{E_2S}}{C_S} \quad C_{E_2SI} = \frac{C_{E_2S} C_I}{k_i}$$

$$\therefore C_{E_2}^0 = \frac{k_m}{C_S} C_{E_2S} + C_{E_2S} + \frac{C_I}{k_i} C_{E_2S}$$

$$C_{E_2S} = C_{E_2}^0 / \left(1 + \frac{k_m}{C_S} + \frac{C_I}{k_i} \right)$$

$$\therefore r = k_2 C_{E_2}^0 / \left(1 + \frac{k_m}{C_S} + \frac{C_I}{k_i} \right)$$

$$= \frac{r_{\max} C_S}{\left(1 + \frac{C_I}{k_i} \right) \left[\frac{k_m}{\left(1 + \frac{C_I}{k_i} \right)} + C_S \right]}$$