

# FUNDAMENTALS OF A CARBON CAPTURE PROCESS: *UNIT OPERATIONS*

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# GOALS OF THESE LECTURES

- Understand the overall process and the key phenomena and equipment
  - Flow in pipes (momentum transfer)
    - pipes, pumps, tanks, fittings and meters
  - Heat transfer between fluids (energy transport)
    - heat exchangers, boilers and condensers
  - Gas absorption and stripping. (mass transfer)
    - Packed column absorber and stripper

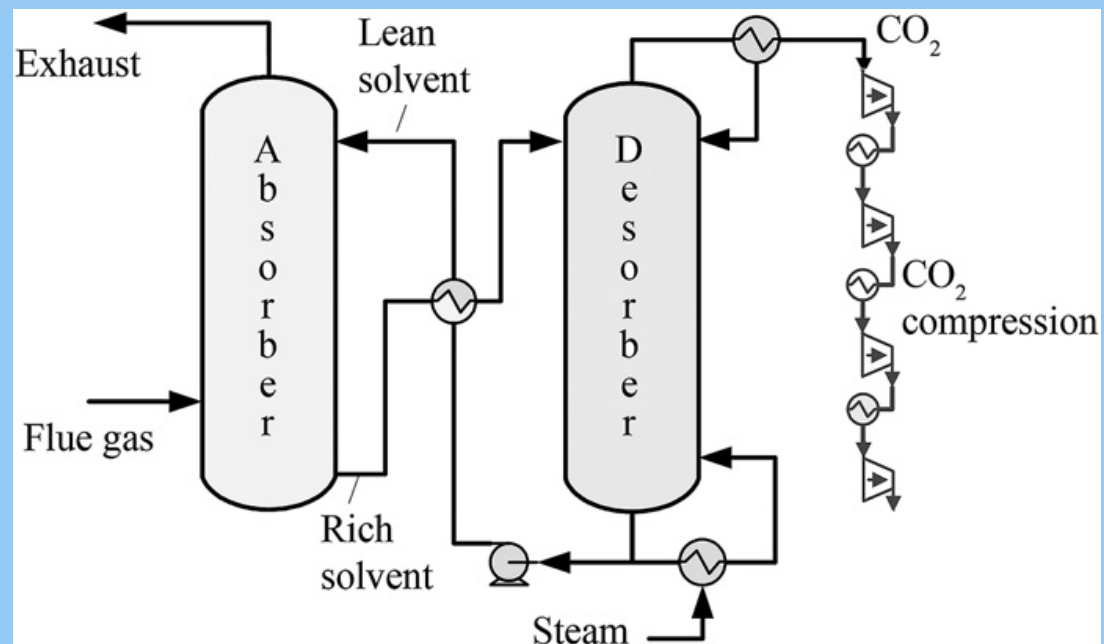
# PLAN FOR TODAY

- Overview of CO<sub>2</sub> absorption
  - Motivation and need for the process
  - How it works
- Description of fundamental processes that occur
  - fluid flow, heat transfer, mass transfer
- Part I: Fluid mechanics and process fluid flows.

# CARBON DIOXIDE ABSORPTION FROM A GAS MIXTURE

- Why do: To get “pure” CO<sub>2</sub>
- Reversible, cyclical process:
  - CO<sub>2</sub> (selectively) dissolves in (lean) MEA solution in the absorber
    - reversible chemical reaction greatly increases solvent capacity and selectivity
  - MEA solution is pumped to the “stripper” where heat (from steam) is used to reduce the CO<sub>2</sub> solubility (and reverse the reaction) so that CO<sub>2</sub> (now) without N<sub>2</sub> will come off.
- Usually need to hit a “spec” on CO<sub>2</sub> emitted.
- Need efficient contacting of gas and liquid
- CO<sub>2</sub> capacity per mass of solvent significantly influences the cost
- Energy to regenerate influences cost

# PROCESS OF INTEREST



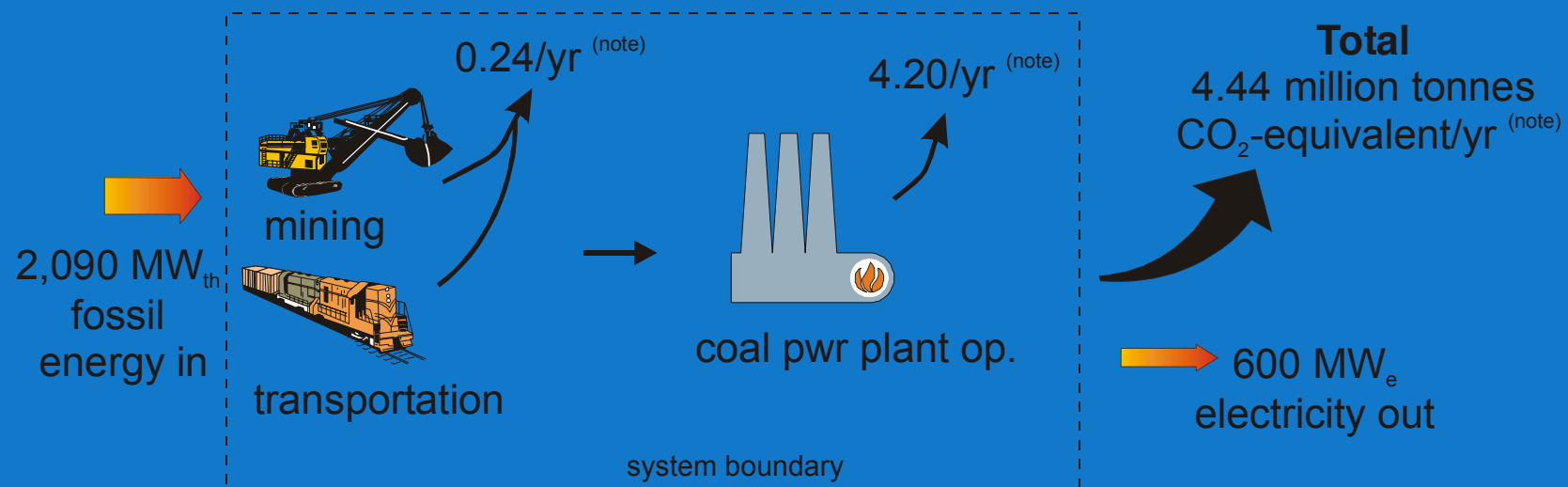
**Fig. 1.** Schematic diagram of absorption section for CO<sub>2</sub> scrubbing with MEA and DGA solutions [10].

# WHY SCRUB CO<sub>2</sub>?

- Natural gas clean up
  - Very large volumes of gas, low concentration of CO<sub>2</sub> (but at elevated pressure)
- Production of hydrogen (also at some elevated pressure)
  - $C + 2H_2O \longrightarrow CO_2 + 2 H_2$
  - $CH_4 + H_2O \longrightarrow CO + 2 H_2$
  - $CO + H_2O \longrightarrow CO_2 + H_2$
- Life support (1 ATM)
- Clean up of combustion gases (~1 ATM coming in.)
  - ~3 mol% (CO<sub>2</sub>) from natural gas, 10-15% from coal

# HAVE TO HAVE A GOOD REASON...

**Figure 1: Coal-fired Power Plant Prior to CO<sub>2</sub> Sequestration (600 MW)**

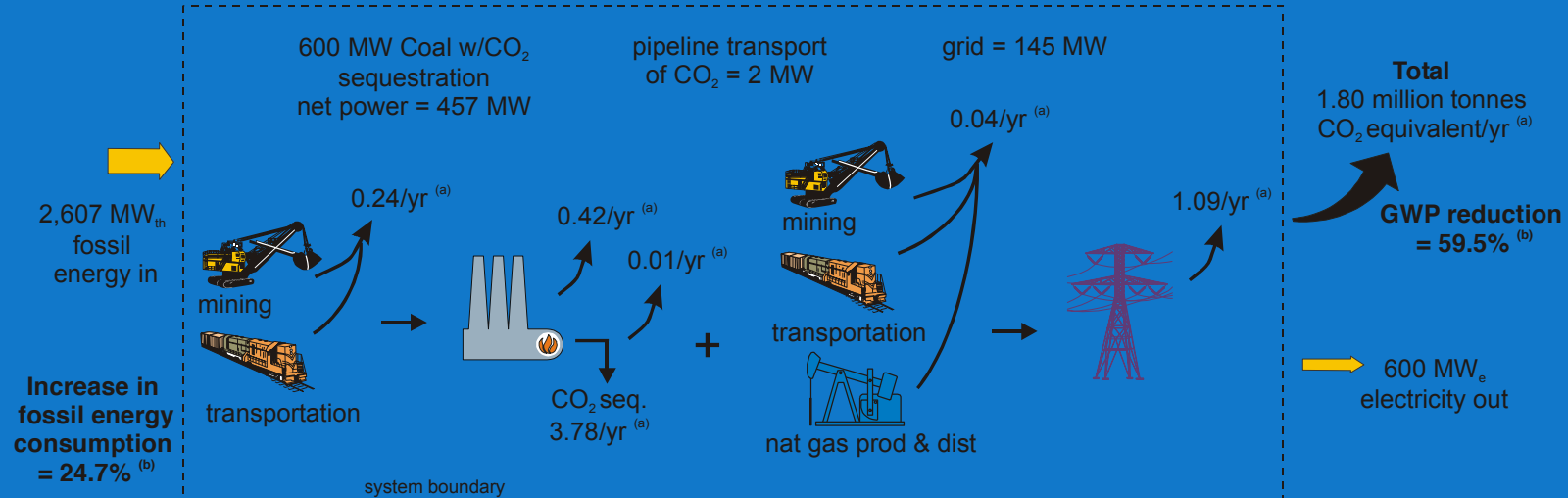


Note: GHGs (CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub>O) expressed in million tonnes CO<sub>2</sub>-equivalents/yr at 100% capacity

# 25% MORE ENERGY IS NEEDED WITH SEQUESTRATION

**Figure 3: Coal-fired Power Plant with CO<sub>2</sub> Sequestration and 145 MW of Grid Capacity Added to Maintain 600 MW**

(U.S. mid-continental grid mix is 64.7% coal, 5.1% lignite, 18.4% nuclear, 10.3% hydro, 1.4% natural gas, and 0.1% oil)



Notes: (a) GHGs (CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub>O) expressed in million tonnes CO<sub>2</sub>-equivalents/yr at 100% capacity; (b) Change in GWP and change in fossil energy consumption compared to reference

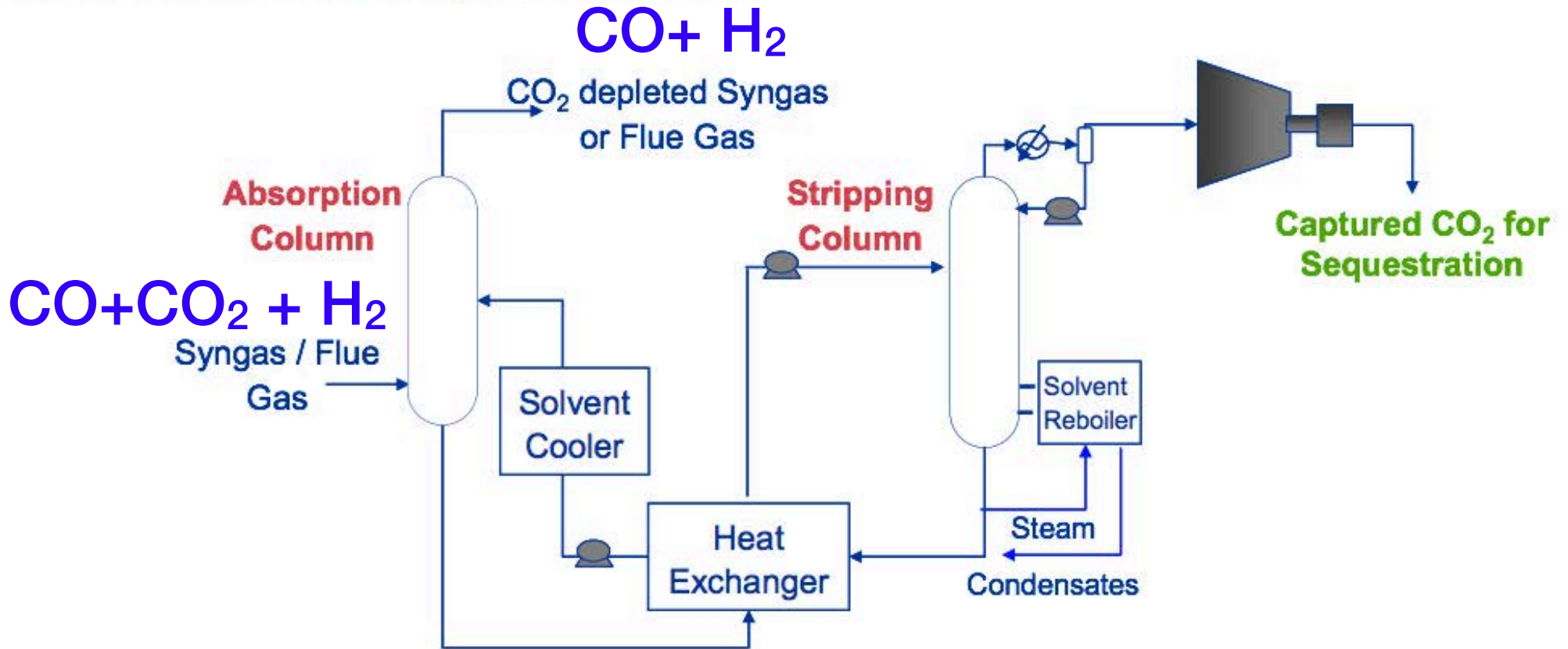


# OTHER APPLICATIONS FOR CO<sub>2</sub> SCRUBBING



# HYDROGEN PRODUCTION

## Amine based Absorption Solution



# METHODS FOR CO<sub>2</sub> SEPARATION

- Membranes
- Absorption into basic solutions (carbonate, hydroxides)
- Absorption into amines
- Solid bed adsorption
- Cryogenic distillation

The Scientific World Journal

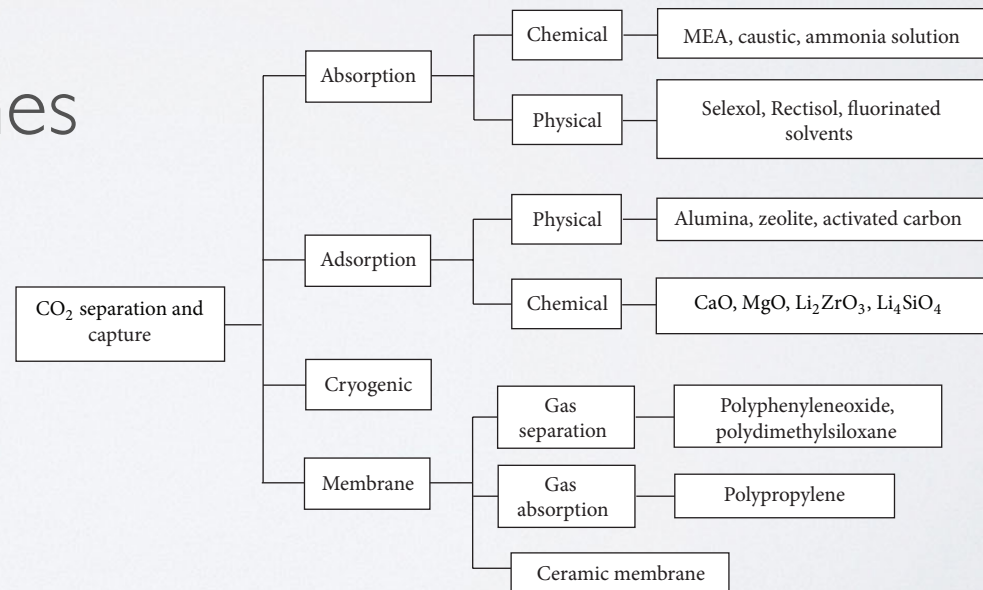
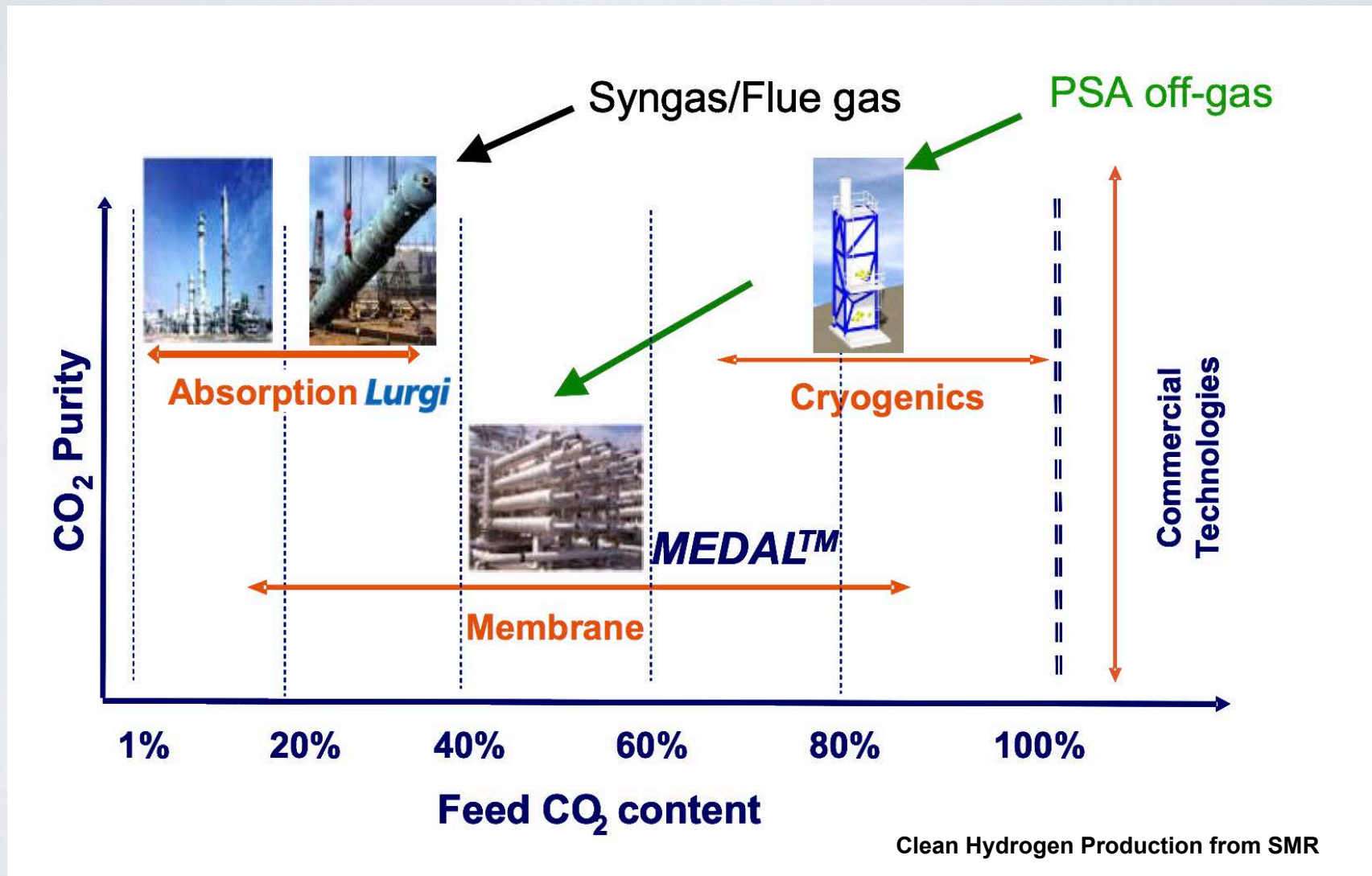
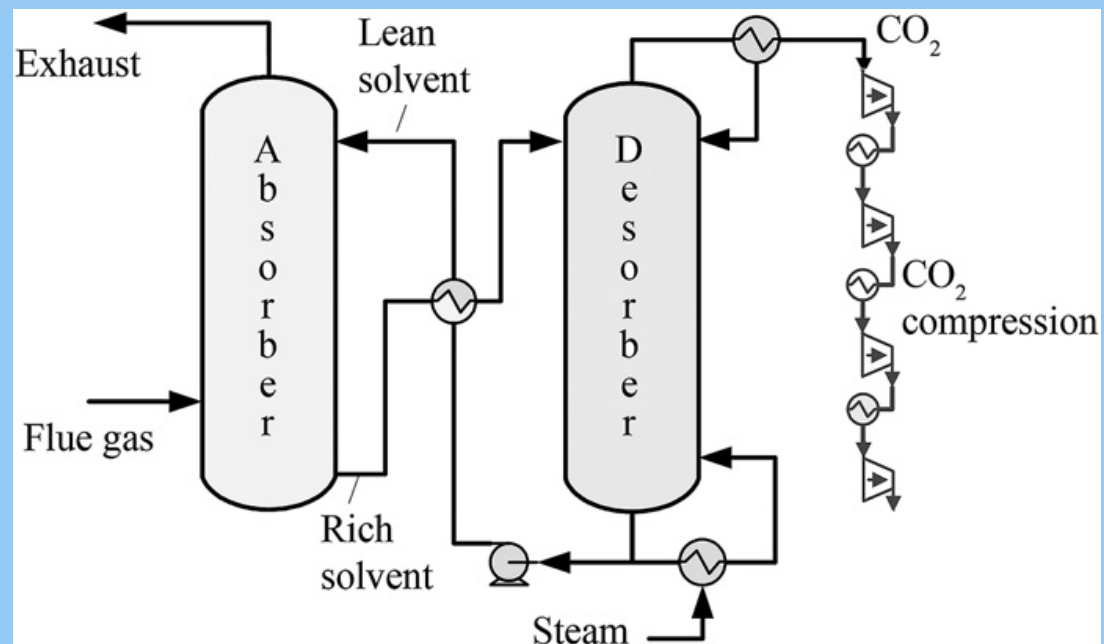


FIGURE 4: Different technologies for CO<sub>2</sub> separation [29].

# COMPARING SEPARATION METHODS



# PROCESS OF INTEREST



**Fig. 1.** Schematic diagram of absorption section for CO<sub>2</sub> scrubbing with MEA and DGA solutions [10].

# SIGNIFICANT COMPRESSION IS NEEDED

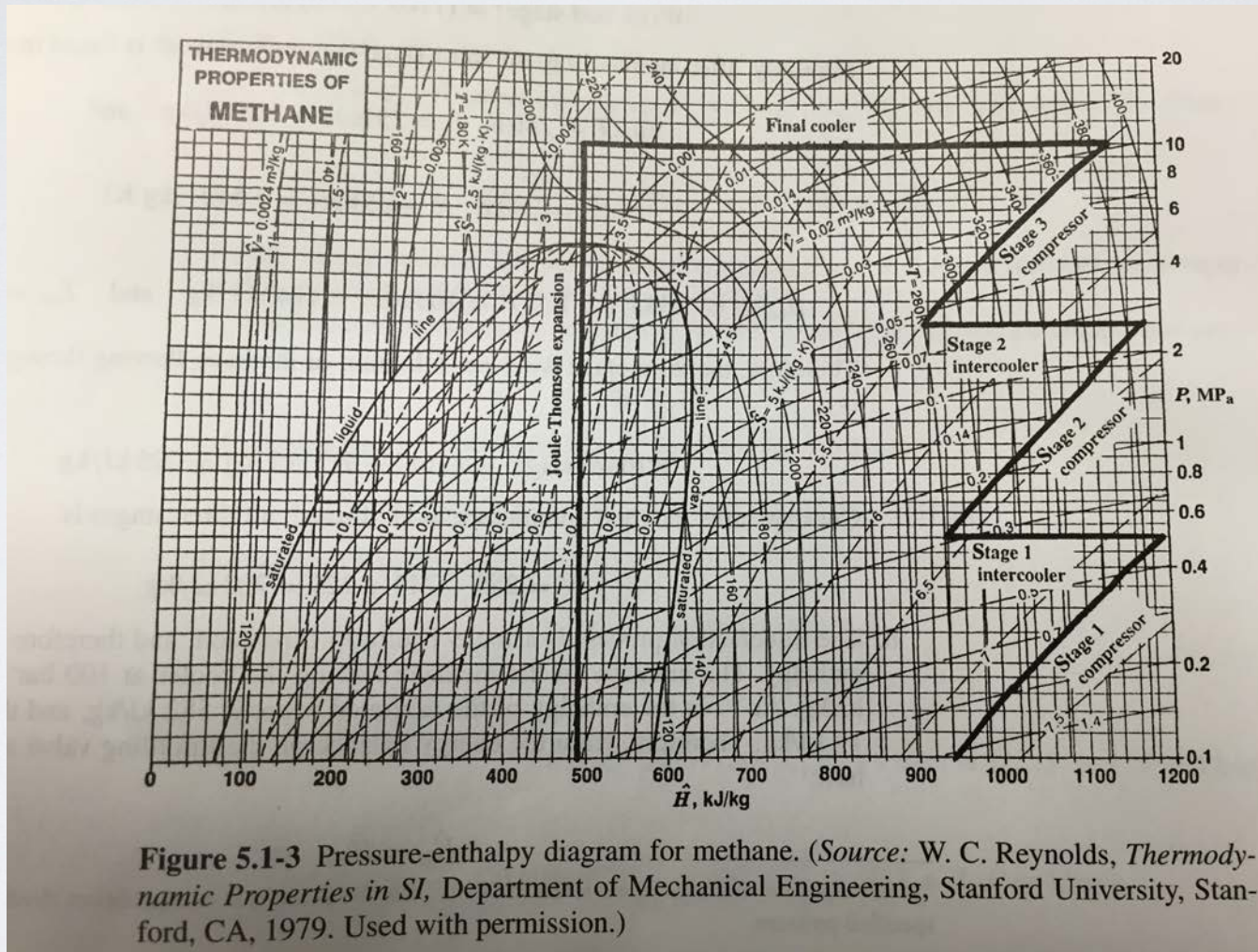
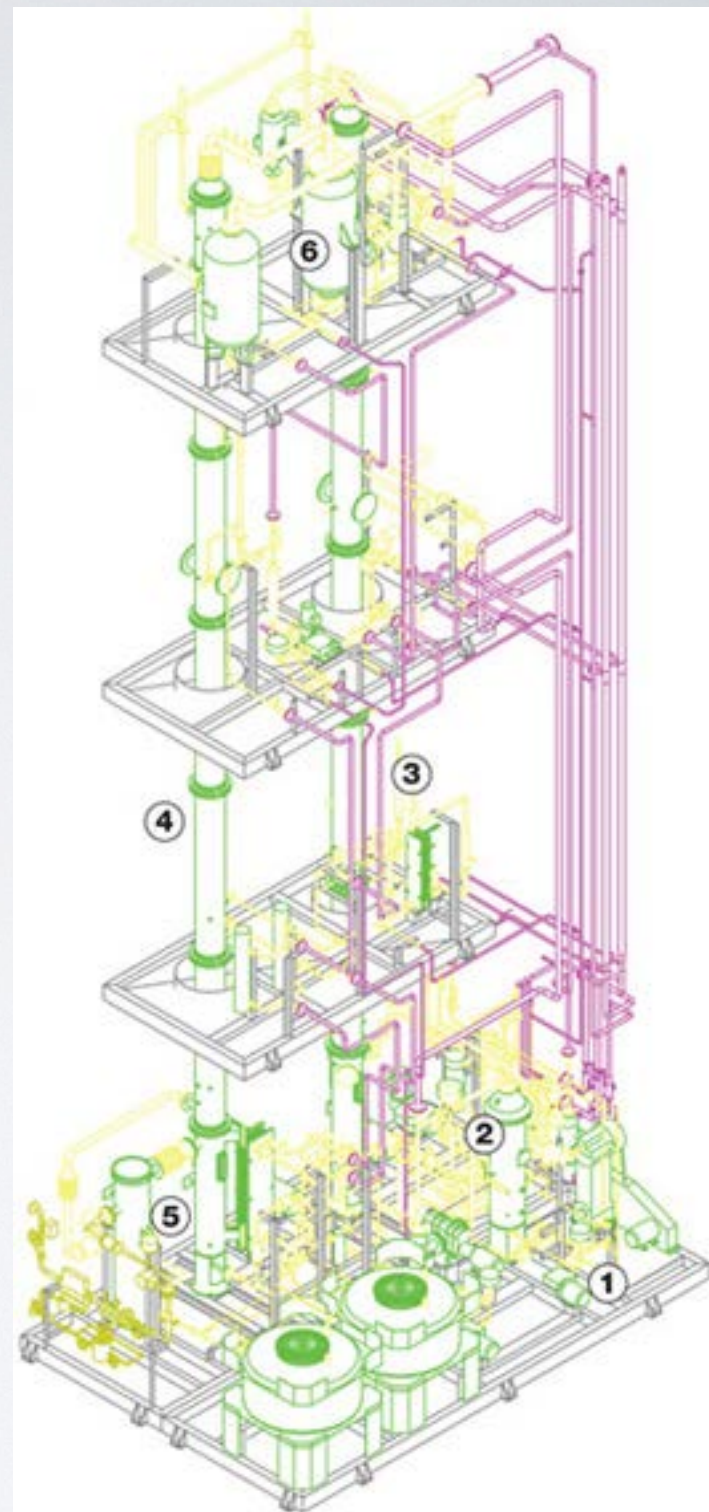


Figure 5.1-3 Pressure-enthalpy diagram for methane. (Source: W. C. Reynolds, *Thermodynamic Properties in SI*, Department of Mechanical Engineering, Stanford University, Stanford, CA, 1979. Used with permission.)

# PILOT PLANT FACILITY



# SCHEMATIC OF IMPERIAL PILOT PLANT





# PILOT PLANT



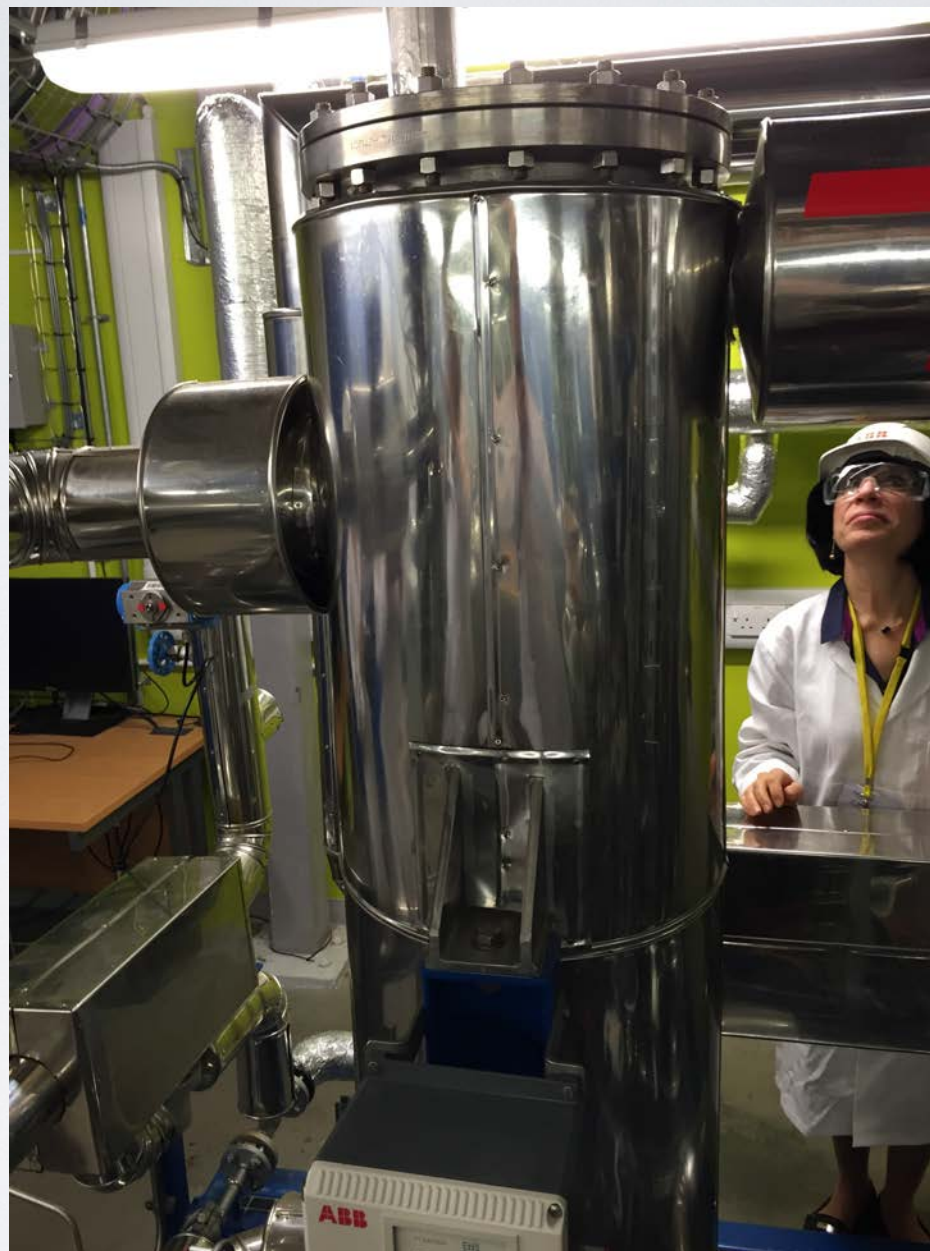
# THE TWO COLUMNS



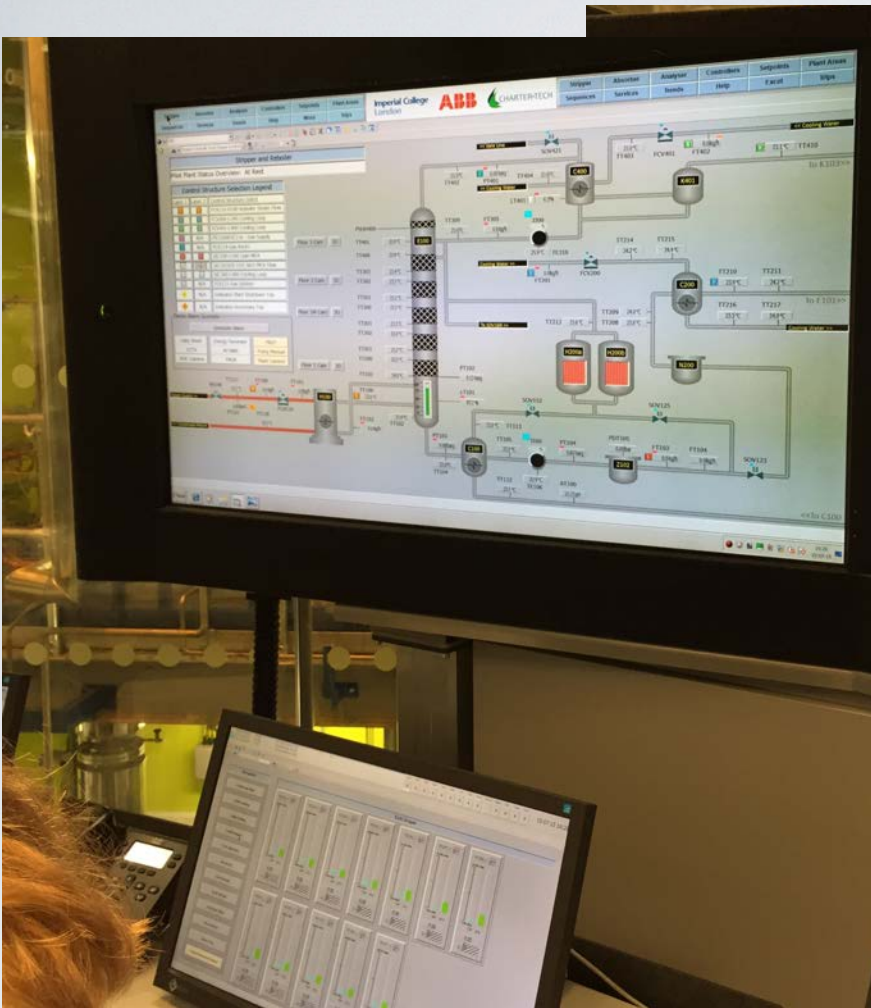
# STUDENTS WORKING IN PLANT



# PROFESSOR SADDAWI INSPECTS THE REBOILER!



# CONTROL ROOM



# LOTS OF SENSORS FOR “CONTROL”



# PROCESS DIAGRAM

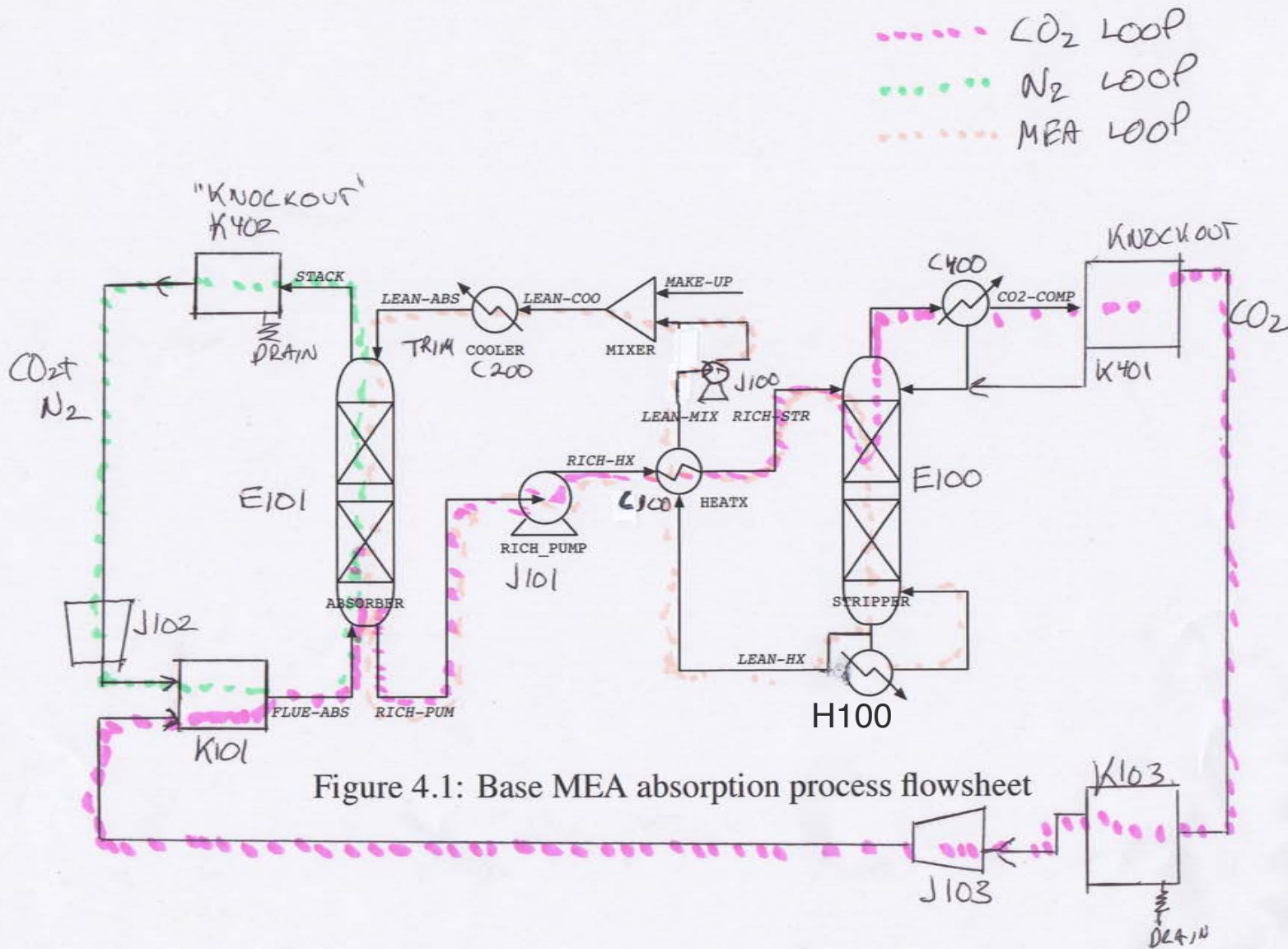
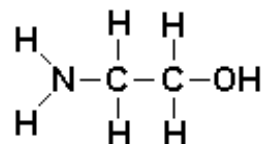


Figure 4.1: Base MEA absorption process flowsheet

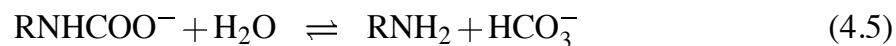
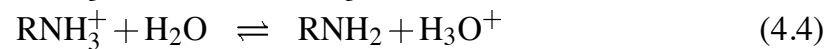
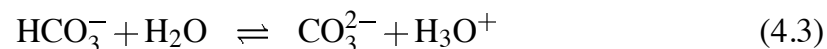
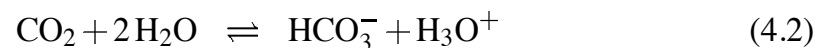
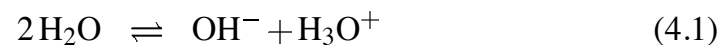
# SOLVENT

- Monoethanolamine (15% in water)



monoethanol-amine (MEA)

- Reactions with  $\text{CO}_2$  and water





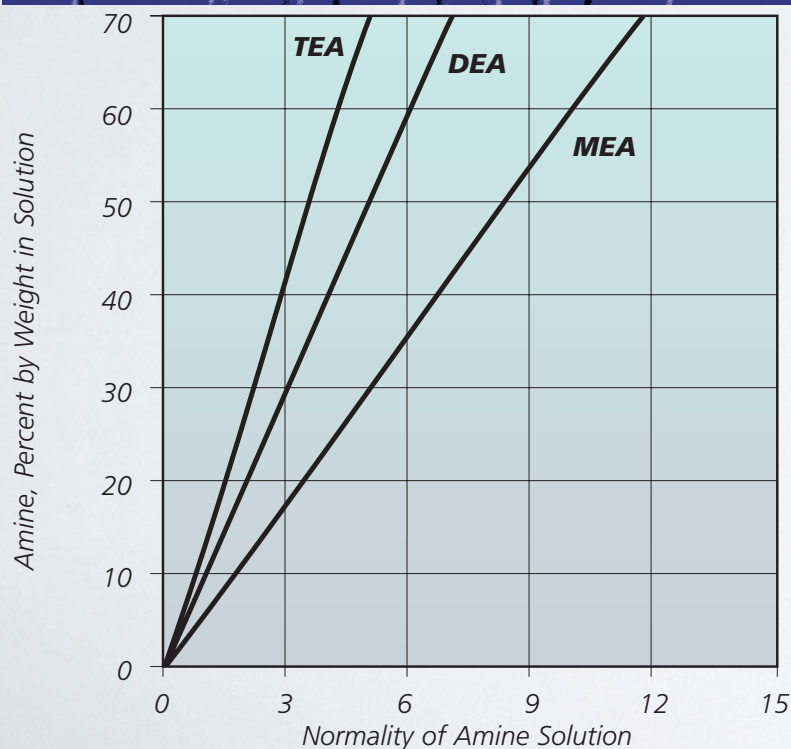
# ETHANOLAMINES

DOW

Monoethanolamine

Diethanolamine

Triethanolamine



**Table 1 • Typical Properties of DOW Ethanolamines**

	Monoethanolamine	Diethanolamine	Triethanolamine
Formula	$\text{H}_2\text{NCH}_2\text{CH}_2\text{OH}$	$\text{HN}(\text{CH}_2\text{CH}_2\text{OH})_2$	$\text{N}(\text{CH}_2\text{CH}_2\text{OH})_3$
Molecular Weight	61.08	105.14	149.19
Apparent Sp. Gr. at 20/20°C	1.017	1.092 <sup>(e)</sup>	1.126 <sup>(f)</sup>
$\Delta\text{Sp. Gr.}/\Delta t$ at 10 to 80°C	0.00080	0.00065 <sup>(b)</sup>	0.00059
Boiling Point at 760 mm Hg, °C	170.4	268 <sup>(c)</sup>	335 <sup>(c)</sup>
at 50mm Hg, °C	101	182	245 <sup>(c)</sup>
at 10mm Hg, °C	71	150	205
Vapor Pressure at 20°C, mm Hg	<1	<0.01	<0.001
Freezing Point, °C(°F)	10.5 (50.9)	28.0 (82.4)	21.6 (70.9) <sup>(e)</sup>
Absolute Viscosity at 20°C, cP	24.1	—	921 <sup>(f)</sup>
at 30°C, cP	16.2	380	404
Solubility at 20°C, % by wt			
In Water	Complete	Complete <sup>(f)</sup>	Complete <sup>(f)</sup>
Water In	Complete	—	Complete <sup>(f)</sup>
Solubility in Organic Liquids at 25°C, % by wt			
Acetone	Complete	Complete <sup>(f)</sup>	Complete
Benzene	0.6	0.03	2
Carbon Tetrachloride	0.1	0.01	Complete
Ethyl Ether	0.7	0.5	2
Heptane	0.1	0.03	<0.03
Methanol	Complete	Complete <sup>(f)</sup>	Complete
Surface Tension, dynes/cm	48.3 <sup>(d)</sup>	48.5 <sup>(g)</sup>	48.9 <sup>(d)</sup>
Refractive Index, $n_D^{20}$	1.4539	1.4747 <sup>(g)</sup>	1.4852 <sup>(f)</sup>
$\Delta n_D/\Delta t$ at 20 to 40°C per °C	0.00034	0.00027 <sup>(b)</sup>	0.00020
Flash Point, °C (°F)	96 (205) <sup>(h)</sup>	191 (375) <sup>(h)</sup>	208 (407) <sup>(h)</sup>

(a) At 30/20°C

(b) At 35 to 65°C

(c) Extrapolated (decomposes)

(d) At 25°C

(e) Supercools easily

(f) Supercooled liquid

(g) At 30°C

(h) Determined by ASTM Method D 93, using the Pensky-Martens Closed Cup

# DATA FOR CO2 INTO MEA

14-10

GAS ABSORPTION

**Table 14-37A. Smoothed Values for Solubility of Carbon Dioxide in 15.3 Weight Per Cent Monoethanolamine**

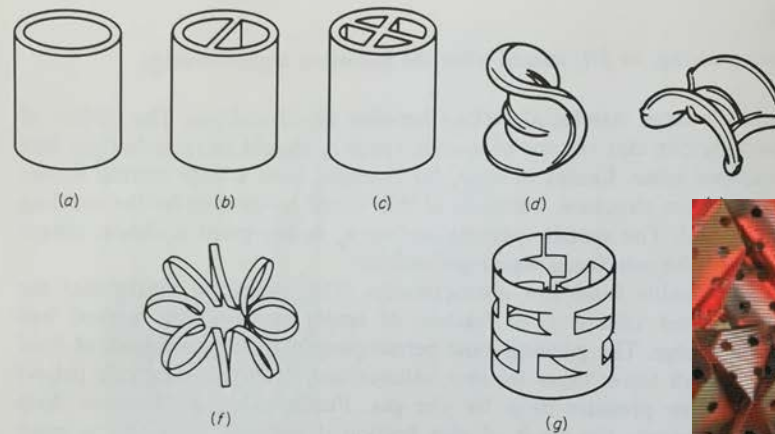
Partial pressure CO <sub>2</sub> , mm. Hg	Moles carbon dioxide per mole amine					
	40°C.	60°C.	80°C.	100°C.	120°C.	140°C.
1	0.383	.....	.....	0.096		
5	.438	.....	.....	.152		
10	.471	0.412	.....	.194		
30	.518	.459	0.379	.265		
50	.542	.482	.405	.299		
70	.558	.498	.422	.322	0.200	
100	.576	.516	.442	.347	.227	0.109
200	.614	.552	.481	.393	.281	.162
300	.639	.574	.505	.423	.314	.194
400	.657	.591	.523	.442	.336	.219
500	.672	.605	.538	.458	.355	.237
600	.686	.615	.550	.472	.370	.254
760	.705	.631	.566	.489	.390	.275
1000	.727	.650	.584	.509	.413	.300
2000	.....	.702	.637	.562	.476	.366
3000	.....	.....	.669	.596	.513	.408
5000	.....	.....	.712	.641	.562	.464
7000	.....	.....	.742	.672	.597	.500

**Table 14-36A. Equilibrium Data for Monoethanolamine Solutions**

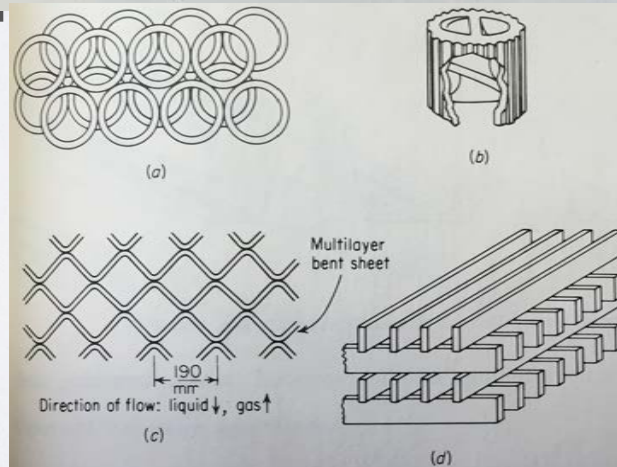
Temp., °C.	Normality of amine	Partial pressure of CO <sub>2</sub> mm. Hg	Liquid concentration, moles CO <sub>2</sub> per mole amine
0.0	0.5	745.8	1.110
.0	.5	256.3	0.990
.0	.5	45.3	.817
.0	.5	10.6	.675
25.0	.5	735.7	1.004
25.0	.5	251.8	0.886
25.0	.5	99.6	.795
25.0	.5	44.2	.720
25.0	.5	10.8	.607
50.0	.5	661.3	.880
50.0	.5	228.3	.757
50.0	.5	40.1	.596
75.0	.5	475.8	.685
75.0	.5	130.3	.584
75.0	.5	50.0	.476
0.0	2.0	754.4	.900
.0	2.0	206.1	.776
.0	2.0	79.4	.718
.0	2.0	11.4	.601
25.0	2.0	736.4	.795
25.0	2.0	252.2	.697
25.0	2.0	98.6	.623
25.0	2.0	44.2	.589
25.0	2.0	10.6	.527
50.0	2.0	668.2	.698
50.0	2.0	183.1	.607
50.0	2.0	70.9	.556
50.0	2.0	10.1	.489
75.0	2.0	477.0	.560
75.0	2.0	130.6	.474
75.0	2.0	51.1	.430

# PACKED TOWER FOR GAS ABSORPTION

## 190 MASS-TRANSFER OPERATIONS

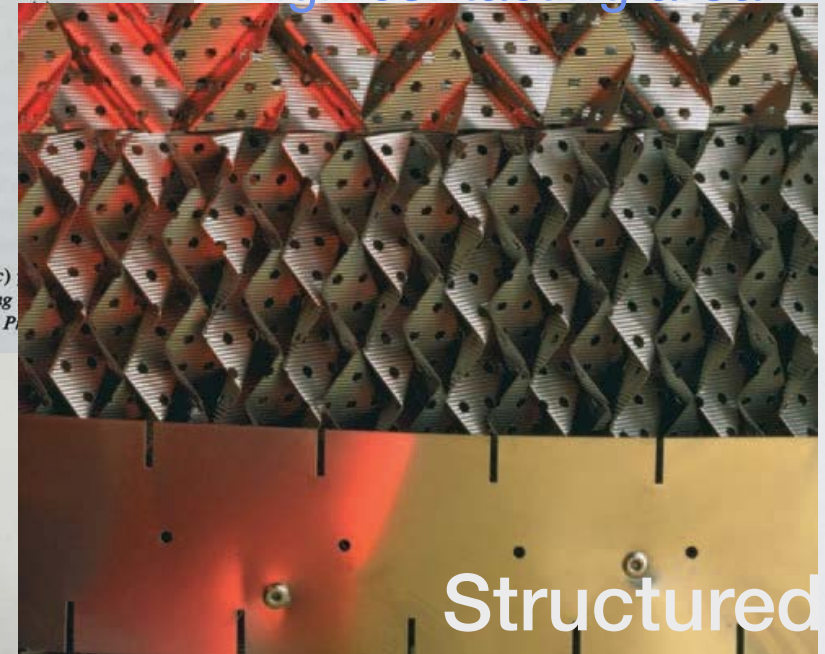


**Figure 6.28** Some random tower packings: (a) Raschig rings, (b) Lessing ring, (c) Berl saddle (courtesy of Maurice A. Knight), (e) Intalox saddle (Chemical Processing Norton Co.), (f) Tellerette (Ceilcote Company, Inc.), and (g) pall ring (Chemical P. Division, Norton Co.).



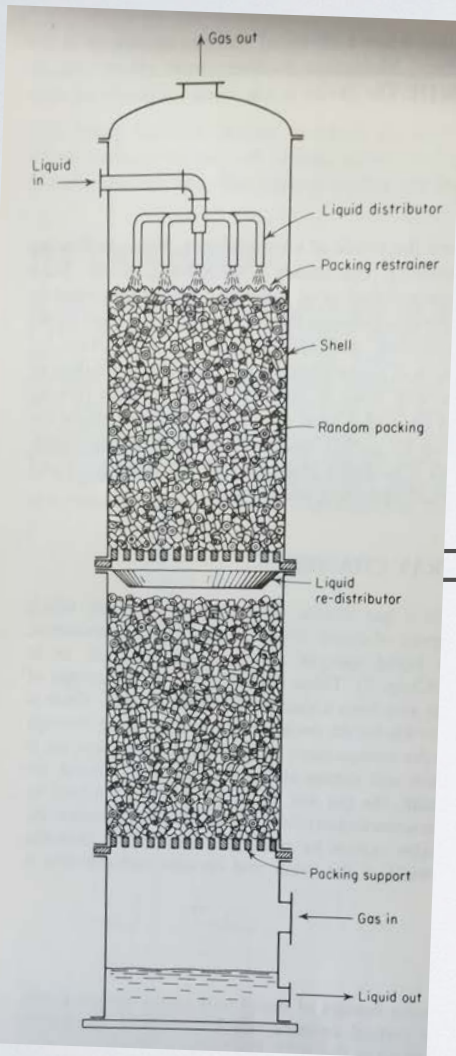
**Figure 6.29** Regular, or stacked, packings: (a) Raschig rings, stacked staggered (top view), (b) double spiral ring (Chemical Processing Products Division, Norton Co.), (c) section through expanded-metal-lath packing, (d) wood grids.

350 m<sup>2</sup>/m<sup>3</sup>  
high contacting area



Structured

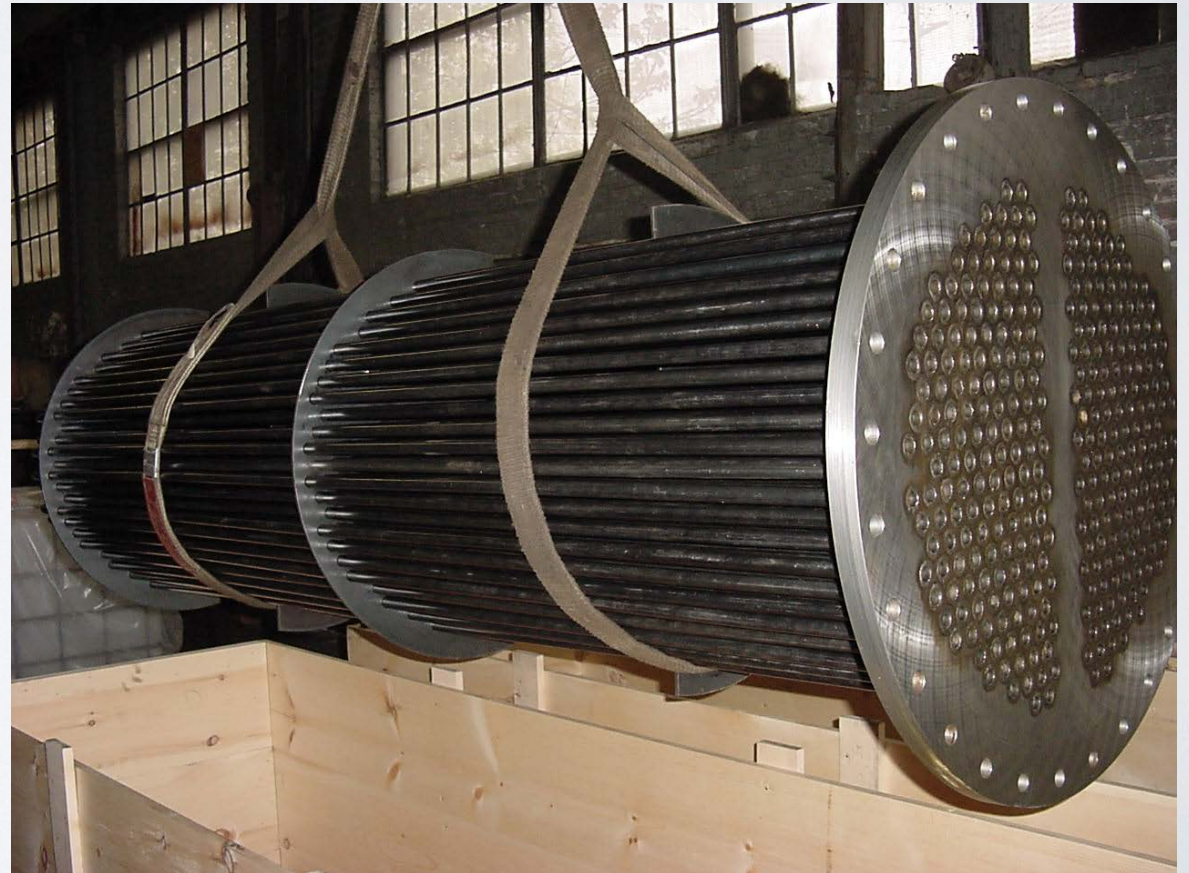
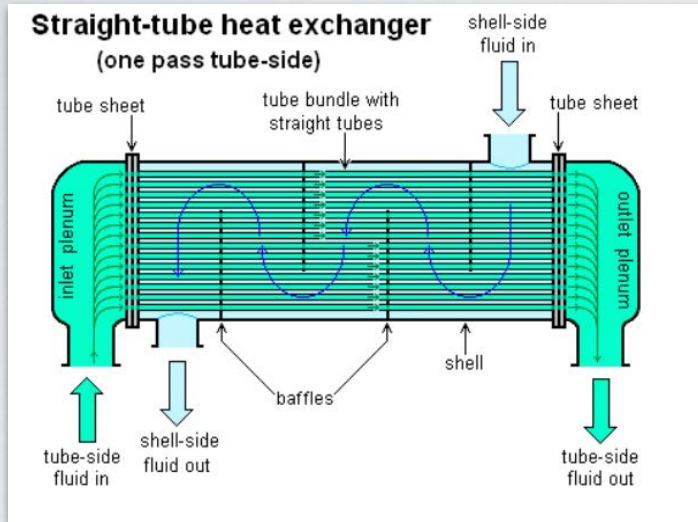
packing in  
absorber



# RANDOM PACKING IN STRIPPING COLUMN



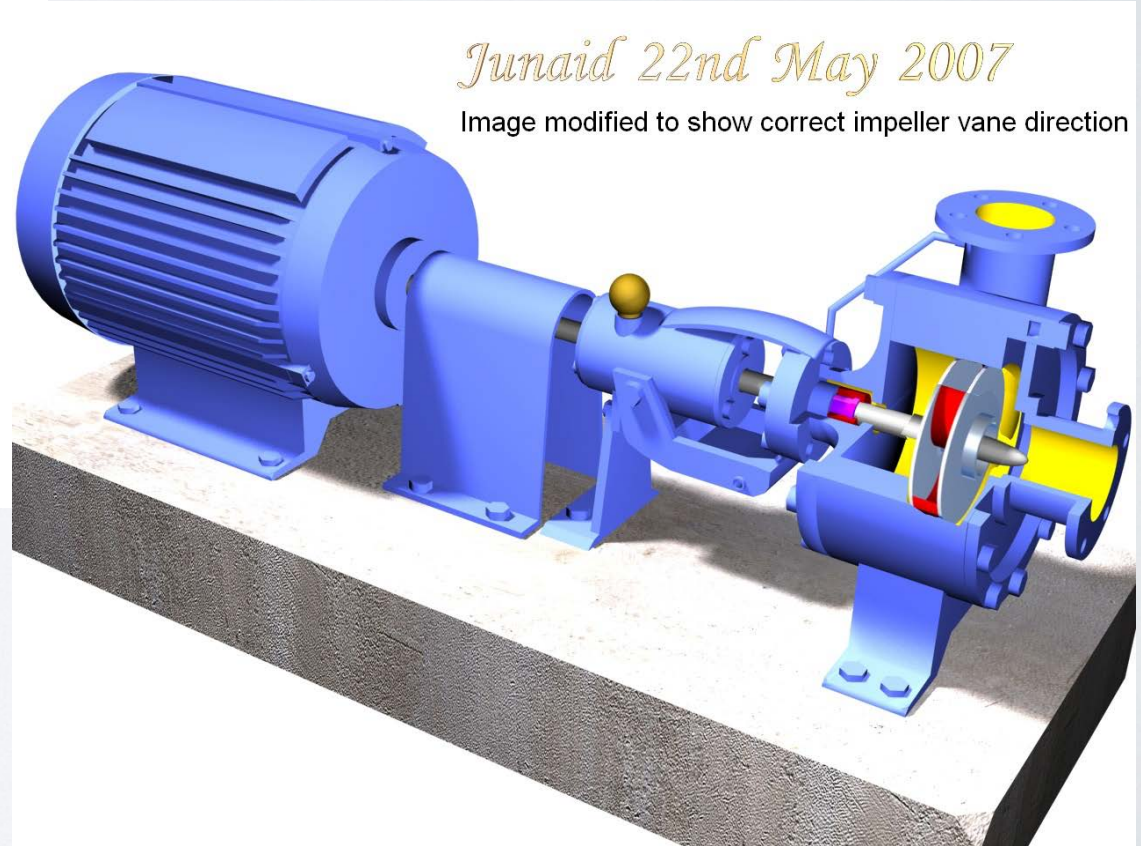
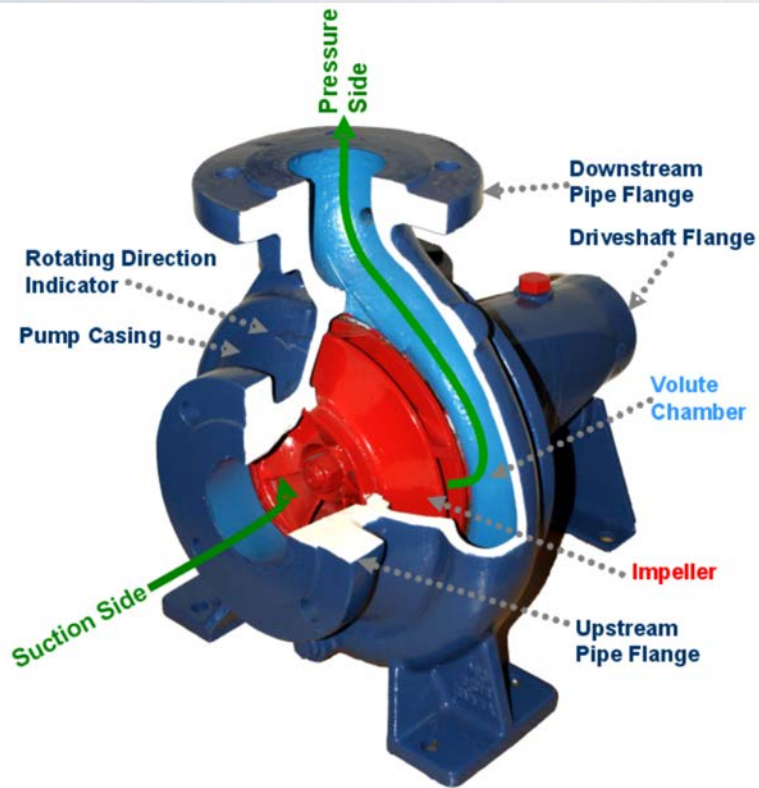
# HEAT EXCHANGERS



# IMPERIAL HEAT EXCHANGERS



# PUMPS



# PUMP FOR MEA

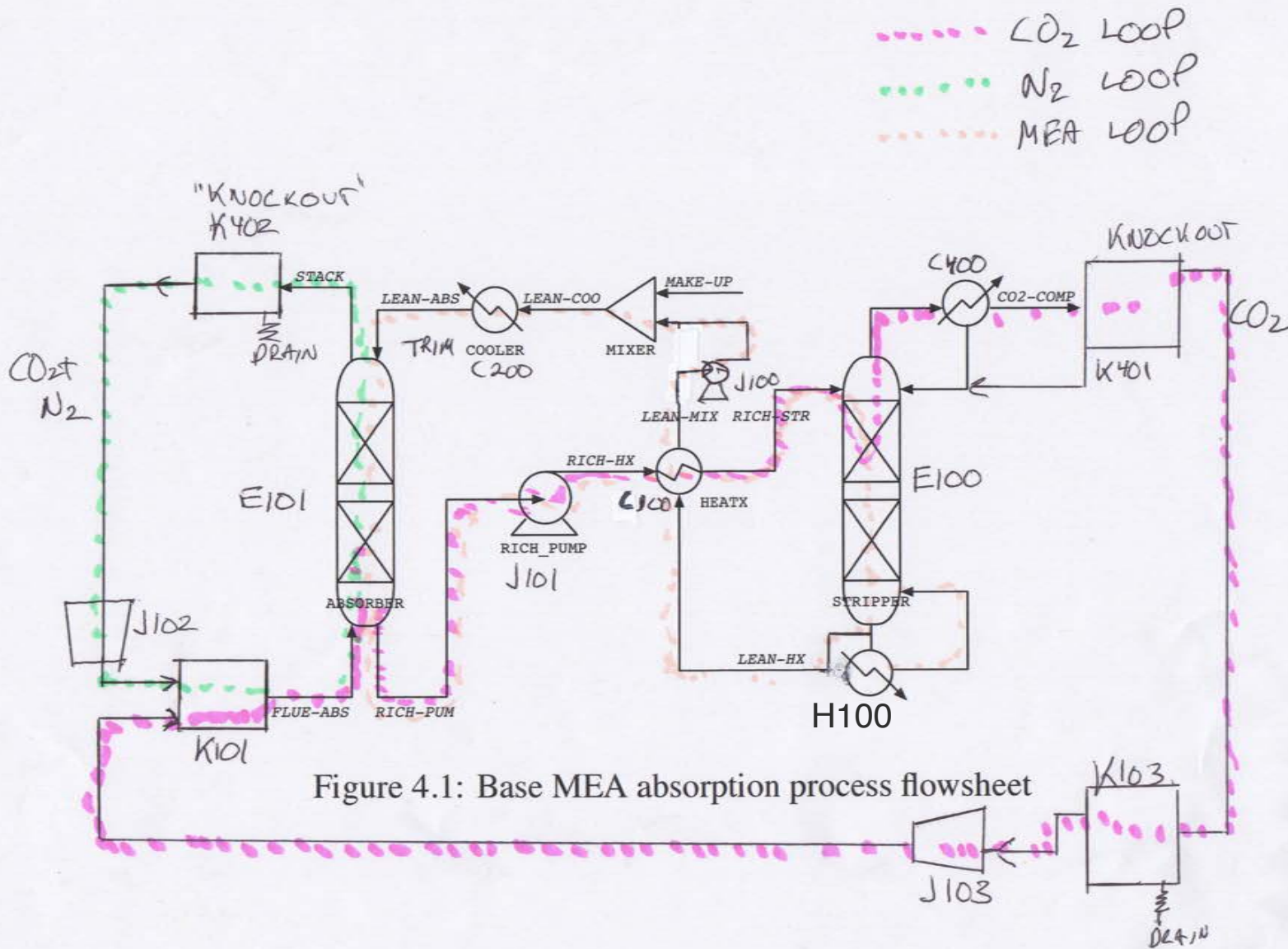




# GAS COMPRESSOR/BLOWER



# PROCESS DIAGRAM



# CARBON DIOXIDE ABSORPTION FROM A GAS MIXTURE

- Why do: To get “pure” CO<sub>2</sub>
- Reversible, cyclical process:
  - CO<sub>2</sub> (selectively) dissolves in (lean) MEA solution in the absorber
    - reversible chemical reaction greatly increases solvent capacity and selectivity
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