

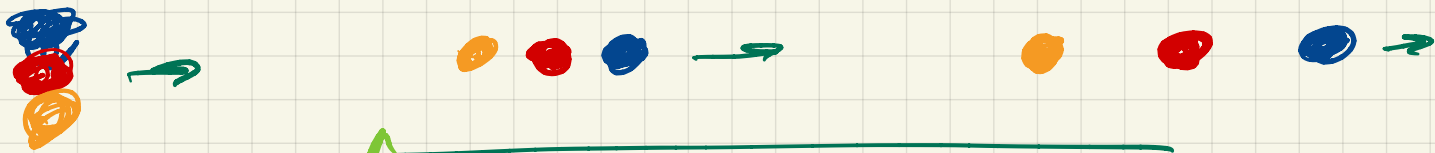
CBE 40448

3/17/21 - ST. PATRICK'S DAY

A REALLY SHORT INTRODUCTION TO

CHROMATOGRAPHY

GENERALLY CAUSES A SEPARATION



MEDIA DEPENDS ON
APPLICATION

OFTEN A PACKED BED
OF PARTICLES



A new general method for designing affinity chromatography processes



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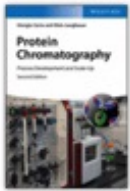
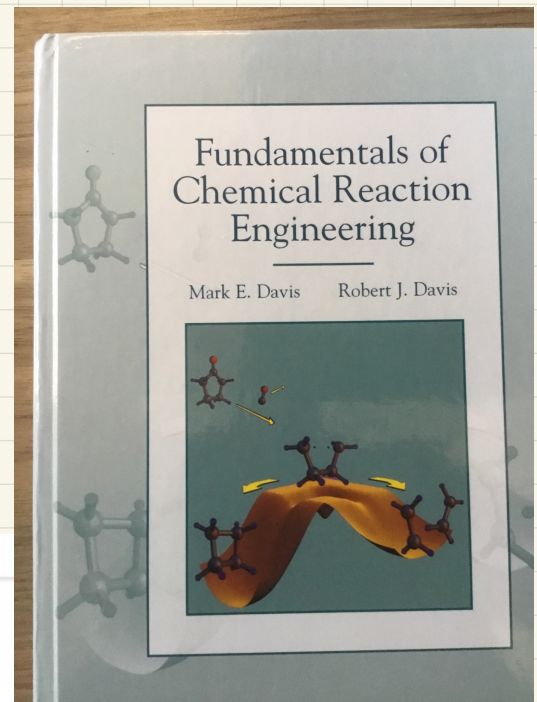
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ARTICLE INFO

ABSTRACT

Article history:

Affinity chromatography is widely used for selectively recovering a target solute from a complex mixture.



Protein Chromatography: Process Development and Scale-Up, Second Edition

Author(s): Giorgio Carta, Alois Jungbauer

First published: 6 March 2020

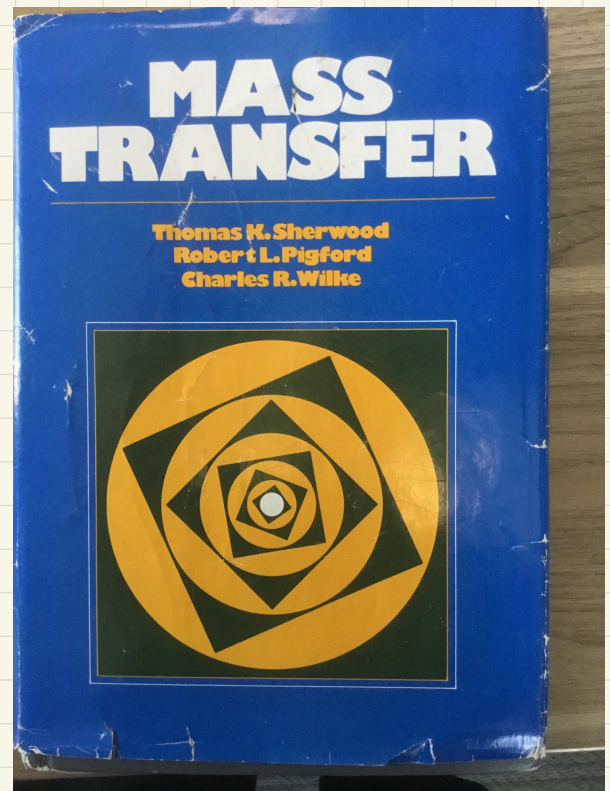
Print ISBN: 9783527346660 | Online

ISBN: 9783527824045

| DOI: 10.1002/9783527824045

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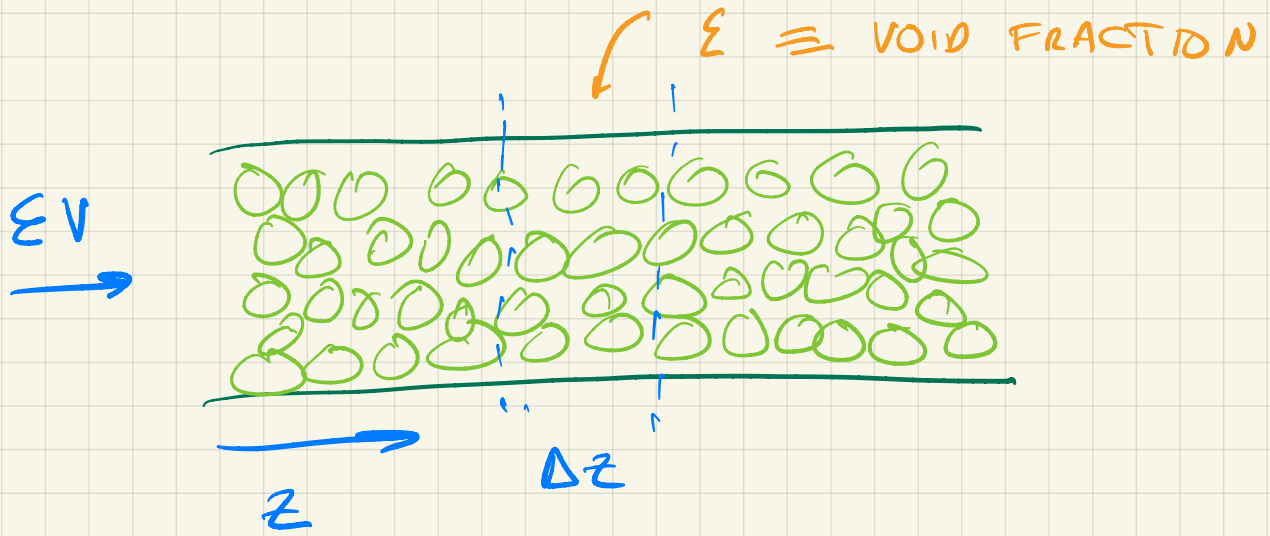


NORMALLY A LIQUID OR GAS
CARRIER PHASE

MIXTURE OF COMPONENTS INTERACTS
WITH "PACKING"

- PHYSICAL ADSORPTION
- CHEMICAL ADSORPTION
- PHYSICAL HINDRANCE

THIS CREATES A DIFFERENCE
IN RATE OF TRAVEL THROUGH
COLUMN FOR VARIOUS COMPONENTS



$C \rightarrow$ CONCENTRATION OF COMPONENT IN FLUID PHASE

$q \rightarrow$ CONCENTRATION OF COMPONENT ON/IN SOLID PHASE

$v \rightarrow$ AVERAGE FLUID VELOCITY IN VOID SPACE OF BED

$\rho_B \rightarrow$ BULK DENSITY OF SOLID PARTICLES

MASS BALANCE:

$$\epsilon \frac{\partial C}{\partial t} + \rho_B \frac{\partial q}{\partial t} + \epsilon v \frac{\partial C}{\partial x} = 0$$

DISPERSION IS NEGLECTED

ACCUMULATION IN FLUID PHASE

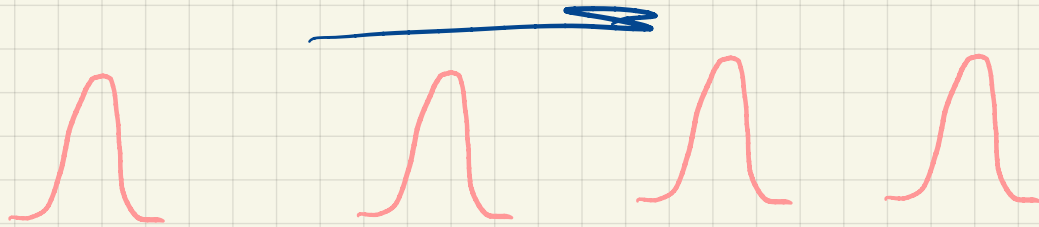
ACCUMULATION ON SOLID PHASE

CONCENTRATION CHANGE ACROSS DIFFERENTIAL SLICE

IF NO EFFECT OF SOLID PHASE!

$$\frac{\partial c}{\partial t} + v \frac{\partial c}{\partial x} = 0$$

SOLUTION IS A TRAVELING WAVE



TO CAUSE A SEPARATION,
SOME INTERACTION WITH SOLID
IS NECESSARY

RATE OF ADSORPTION TO SOLID

$$S_B \frac{\partial q}{\partial t} = k a F(c, q)$$

Annotations for the equation:

- S_B : MASS TRANSFER COEFFICIENT
- $k a$: CONTACT AREA - INCLUDES INSIDE PARTICLES
- $F(c, q)$: EQUILIBRIUM RELATION BETWEEN SOLID & FLUID PHASE

GAS - SOLID EQUILIBRIUM

SIMPLEST MODEL IS LANGMUIR ADSORPTION

- PHYSICAL ADSORPTION
- SINGLE LAYER
- IDEAL GAS . . .

θ \rightarrow FRACTIONAL COVERAGE OF ADSORBENT

q^* = EQUILIBRIUM SOLID CONCENTRATION

p - PARTIAL PRESSURE OF COMPONENT

K \rightarrow RATE CONSTANT FOR ADSORPTION

$$Kp(1-\theta) = K'\theta$$

RATE OF ADSORPTION

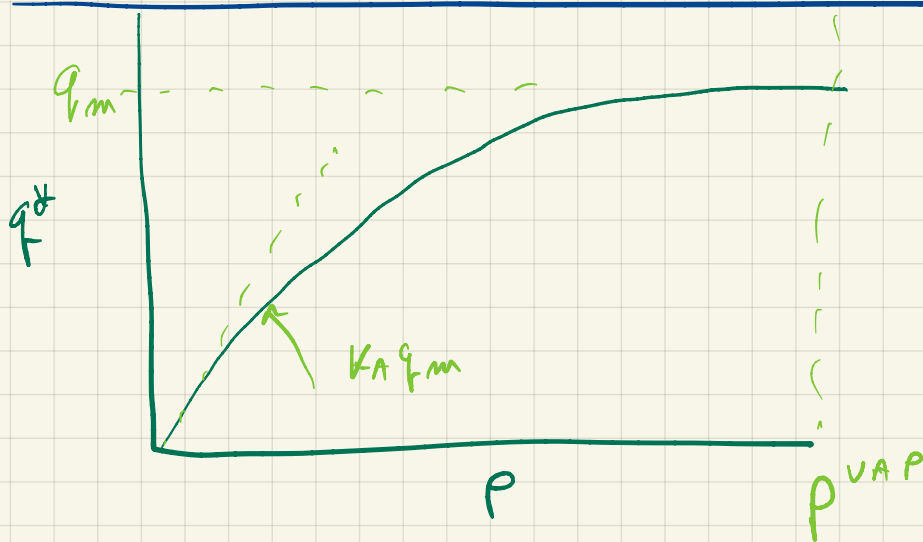
RATE OF DESORPTION

ADSORPTION CONSTANT

$$q^* = q_m \frac{K_A p}{1 + K_A p}$$

MAX COVERAGE

TYPICAL LANGMUIR DIAGRAM



NO LIQUID PHASE SYSTEM OR
MIXTURE WITH "LARGE" MOLECULES
IS REALLY "LANGMUIR"

NEVERTHELESS - IT IS USUALLY
USED ANYWAY !!

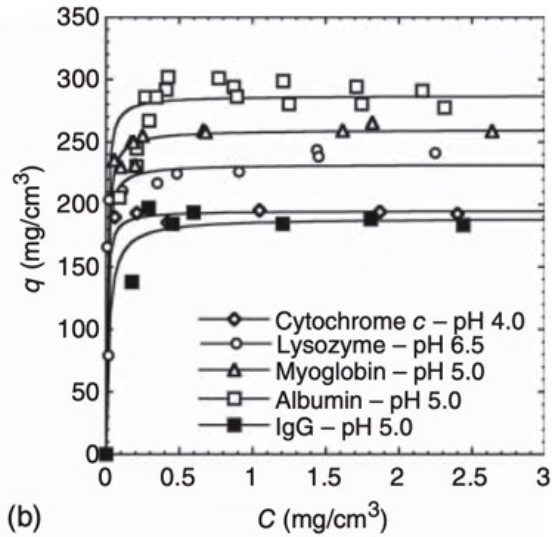
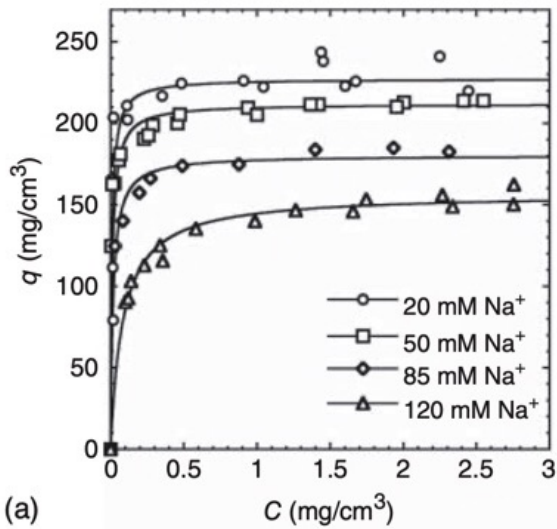
FOR A SPECIFIC PACKING, THERE
IS A MAXIMUM CAPACITY OF
THE ADSORBENT AT FEED
CONCENTRATION

$$q_m^* = \frac{a C_F}{1 + b C_F} = a^* C_F$$

↑
PACKING CONSTANT

ADSORPTION EQ DATA

q^*



q^*

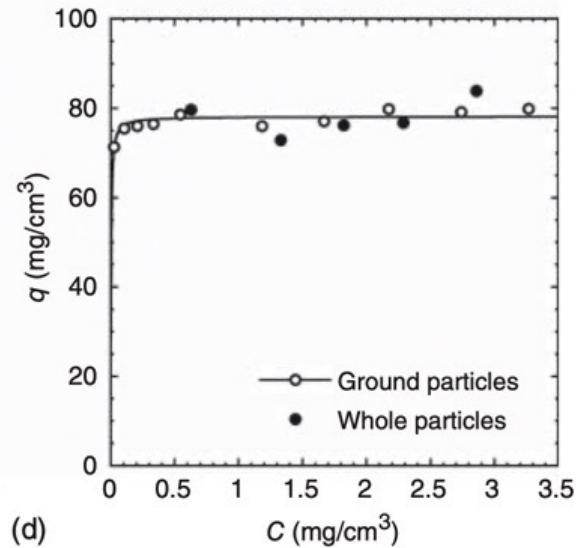
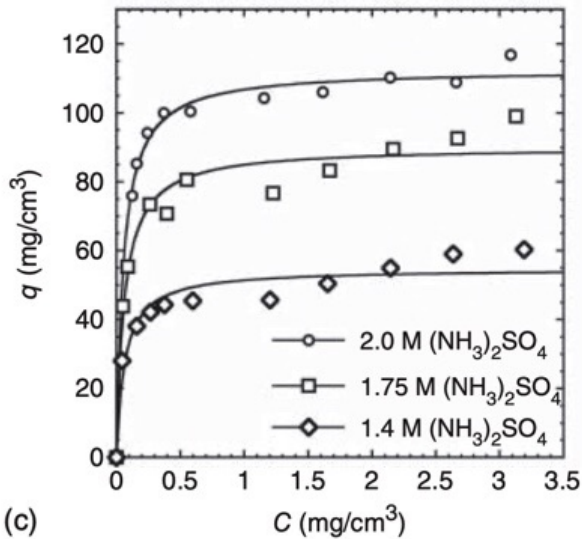


Figure 5.1 Examples of adsorption isotherms for ion exchange chromatography (a, b), hydrophobic interaction chromatography (c), and protein A affinity chromatography (d). The experimental data have been approximated by the Langmuir adsorption isotherm with parameters q_m and K_L fitted at each mobile-phase composition and for each protein. Source: Adapted from Bankston et al. 2008 [2].

IF YOU WANT COMPONENT TO
"STICK", q^* IS NOT A
STRONG FUNCTION OF C

NEXT IDEALIZATION

FAST MASS TRANSFER

$$q^* = f(c)$$

LOCAL
EQUILIBRIUM

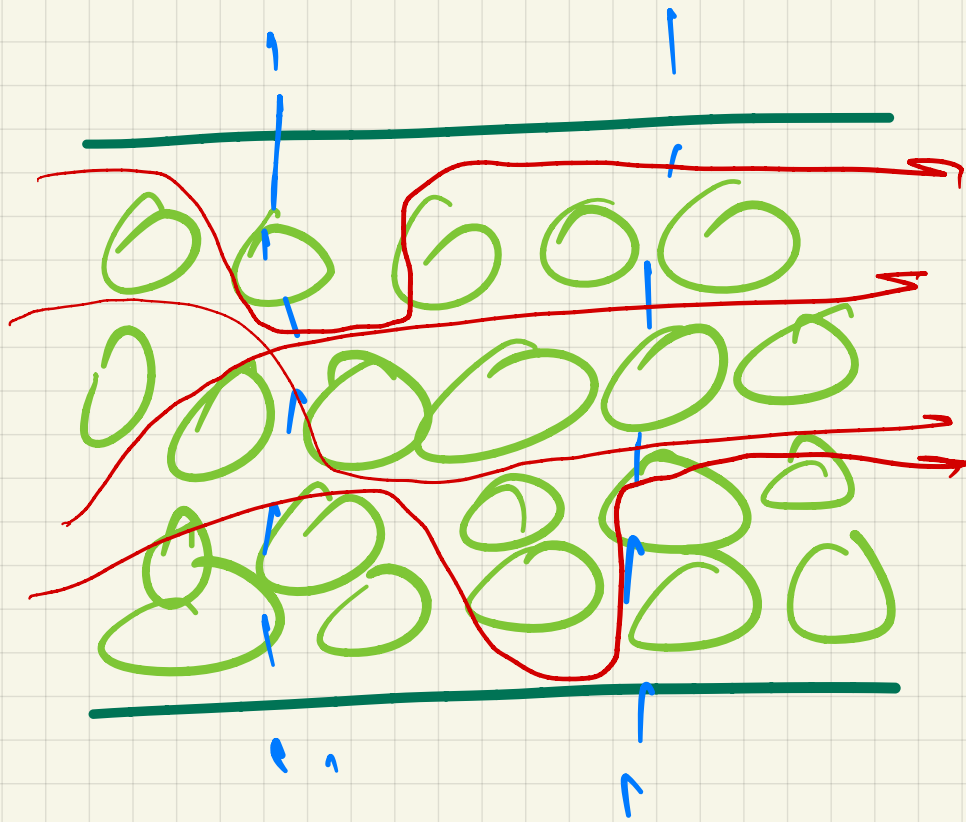
$$\frac{\partial q}{\partial t} = \frac{\partial q^*}{\partial t} = \frac{\partial f(c)}{\partial t} = f'(c)$$

MASS BALANCE

$$\frac{\partial c_i}{\partial t} + \left(\frac{v}{1 + \frac{\rho_0}{\epsilon} f'_i(c)} \right) \frac{\partial c_i}{\partial x} = 0$$

RATE OF
TRAVEL OF
COMPONENT i
THROUGH
BED

LARGER $f'_i(c)$
STRONGER
INTERACTION
SLOWER
TRANSPORT



MANY PATHS THROUGH
BED.

FOR:

- ION EXCHANGE
- AFFINITY CHROMATOGRAPHY

YOU DON'T WANT THIS!

YOUTUBE VIDEO !!
- .

<https://www.youtube.com/watch?v=sKC--1kknTg>

THUS NEED A RESIDENT TIME
 SUCH THAT DIFFUSION TO SURFACE
 OF PARTICLES AND WITHIN
 PARTICLES IS FAST COMPARED
 TO CONVECTION THROUGH

BED !!

SUPERFICIAL VELOCITY

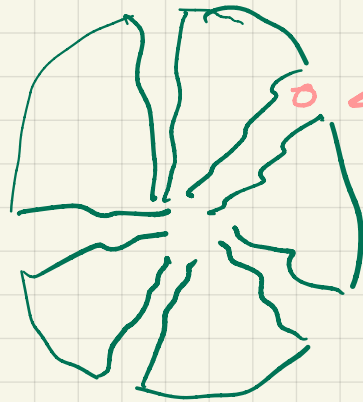
DIAMETER OF PARTICLE

$$Pe = \frac{V L}{D}$$

DIFFUSIVITY OF COMPONENT

$$\sim 10^{-7} \text{ cm}^2/\text{s} !!$$

YOU WOULD
 LIKE THIS
 TO BE
 SMALL
 MAY NOT
 BE



MAY BE KNOWN AS
 DIFFUSION $\rightarrow D_{KA}$

IF YOU
 WANT TO
 USE
 FULL
 CAPACITY
 OF
 PARTICLES!

"THIELE" MODULUS

$$\phi \sim \frac{(L/2)^2 / D_{KA}}{\frac{V}{Z}} < 1$$

$$L/2 = 25 \mu\text{m} = 25 \times 10^{-4} \text{cm}$$

$$D_{KA} = 1 \times 10^{-7} \text{cm}^2/\text{s}$$

$$\text{INTERNAL DIFFUSION TIME} \sim \frac{(25 \times 10^{-4} \text{cm})^2}{1 \times 10^{-7} \text{cm}^2/\text{s}} = 60 \text{S}$$

THE VALUE OF v COULD BE
10 cm/min

SO THE COLUMN NEEDS TO
BE 50 cm OR MORE

FOR INTERNAL CAPACITY
TO BE UTILIZED

WHAT IS PRESSURE DROP?

ERGON EQ!

$$\frac{\Delta P}{Z} = \frac{150 (1-\epsilon)^2 \mu V}{\epsilon^3 L^2}$$

$$= \frac{150 (1-.4)^2}{(.4)^3} \frac{2 \times 10^{-3} \frac{\text{kg}}{\text{m}\cdot\text{s}} (.002 \text{ m/s})}{(50 \times 10^{-6} \text{ m})^2}$$

$$= 50,000 \text{ Pa/m}$$

$$= 1/2 \text{ ATM/m}$$

SO YOU COULD HAVE A LONGER COLUMN OR SMALLER PARTICLES OR FASTER V .

SOME PACKING MATERIALS

LIMIT MAX $\frac{\Delta P}{Z}$

